

Blade/Casing Contacts in Turbomachinery: State of the Art and Recent Developments

Alain Batailly

Laboratory for Acoustics and Vibration
Analysis

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Foreword

I - Rotor/stator interactions

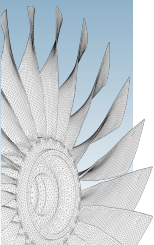
II - Research investigations

III - Industrial applications

IV - Going forward...

References

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I - Rotor/stator interactions

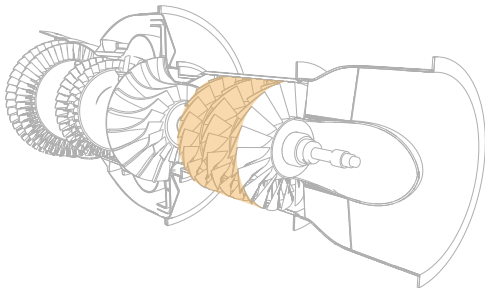
II - Research investigations

III - Industrial applications

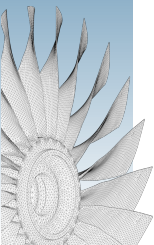
IV - Going forward...

References

- overview of past and on-going research in the field of rotor/stator interactions
- focus on blade-tip/casing interface
 - ① why do manufacturers focus on this interface?
 - ② what are the related research challenges?
 - ③ what could be the practical outcomes of these works?
- current bottlenecks and challenges to tackle



► blade-tip/casing interface in the low-pressure compressor of a helicopter engine





I - Rotor/stator interactions

Overview

Blade/casing interface

Problem-solving strategy

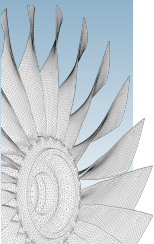
II - Research investigations

III - Industrial applications

IV - Going forward...

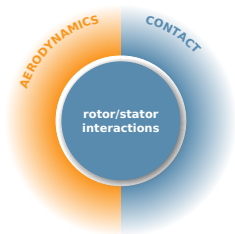
References

1 Rotor/stator interactions





Research context



I - Rotor/stator interactions

Overview

Blade/casing interface

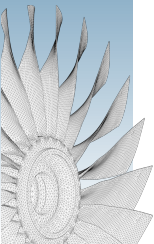
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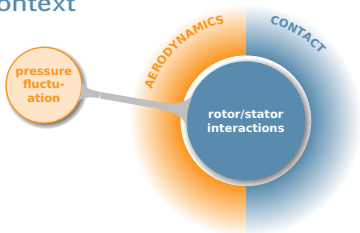
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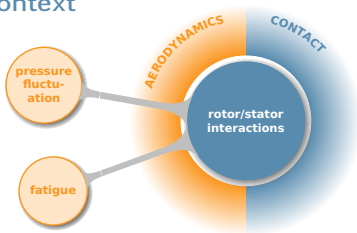


- first investigations with respect to unsteady forces due to airfoil passage ¹
- investigations on propagation of wakes through blade rows ²
- development of experimental and numerical methods in unsteady aerodynamics ³
- led to experimental works related to pressure fluctuations in turbines ⁴

1. N. H. Kemp et al. *Journal of the Aeronautical Sciences* (1953). doi: [10.2514/8.2758](https://doi.org/10.2514/8.2758).
2. M. D. Lefcort. en. *Journal of Engineering for Power* (1965). doi: [10.1115/1.3678275](https://doi.org/10.1115/1.3678275).
3. H. E. Gallus. en. New York, NY: Springer, 1993. doi: [10.1007/978-1-4613-9341-2_23](https://doi.org/10.1007/978-1-4613-9341-2_23).
4. R. P. Dring et al. en. *Journal of Engineering for Power* (1982). doi: [10.1115/1.3227339](https://doi.org/10.1115/1.3227339).



Research context



- impact on the fatigue life of bladed components^{5, 6}
- numerical/experimental comparisons⁷
- development of numerical methods for mistuned bladed disks⁸

5. R. Mailach et al. en. *Journal of Turbomachinery* (2004). doi: [10.1115/1.1791641](https://doi.org/10.1115/1.1791641).

6. R. Mailach et al. en. *Journal of Turbomachinery* (2004). doi: [10.1115/1.1791642](https://doi.org/10.1115/1.1791642).

7. M. B. Schmitz et al. en. Dordrecht: Springer Netherlands, 2006. doi: [10.1007/1-4020-4605-7_9](https://doi.org/10.1007/1-4020-4605-7_9).

8. E. Seinturier et al. en. American Society of Mechanical Engineers Digital Collection, 2009. doi: [10.1115/GT2002-30424](https://doi.org/10.1115/GT2002-30424).



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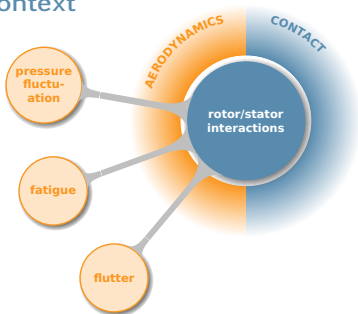
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References

Research context



- developments driven by research in a military context⁹
- development of several numerical methods dedicated to flutter calculations: 2D¹⁰ and 3D¹¹
- vast amount of research on the subject¹²

9. M. F. Platzer et al. 1987, [available online](#).

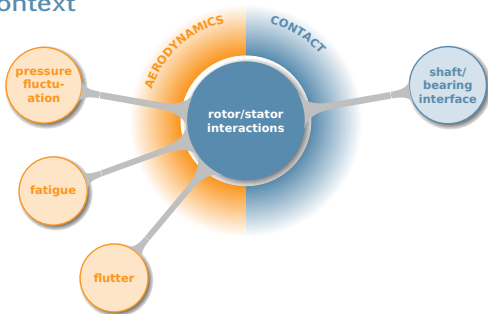
10. J. M. Verdon et al. *AIAA Journal* (1982). doi: 10.2514/3.51186.

11. L. He et al. en. *Journal of Turbomachinery* (1994). doi: 10.1115/1.2929436.

12. K. Isomura et al. en. *Journal of Turbomachinery* (1998). doi: 10.1115/1.2841746.



Research context



- focus on phenomenological models (Jeffcott rotor)¹³
- evidence of complex dynamics behaviors¹⁴
- prediction and characterization of whirl/whip motions¹⁵

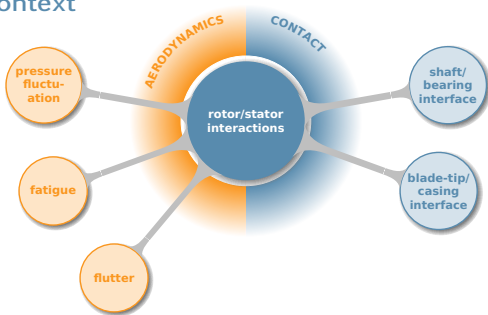
13. D. W. Childs. en. *Journal of Mechanical Design* (1979). doi: [10.1115/1.3454114](https://doi.org/10.1115/1.3454114).

14. F. F. Ehrich. en. *Journal of Vibration, Acoustics, Stress, and Reliability in Design* (1988). doi: [10.1115/1.3269488](https://doi.org/10.1115/1.3269488).

15. A. Muszynska. en. *Journal of Sound and Vibration* (1986). doi: [10.1016/S0022-460X\(86\)80146-8](https://doi.org/10.1016/S0022-460X(86)80146-8).



Research context



- generalization of shaft/bearing systems to bladed rotors¹⁶
- extension of the modelling to blades' torsion modes¹⁷
- development of predictive numerical strategies^{18, 19}

16. J. Padovan et al. en. *Journal of Turbomachinery* (1987). doi: [10.1115/1.3262143](https://doi.org/10.1115/1.3262143).

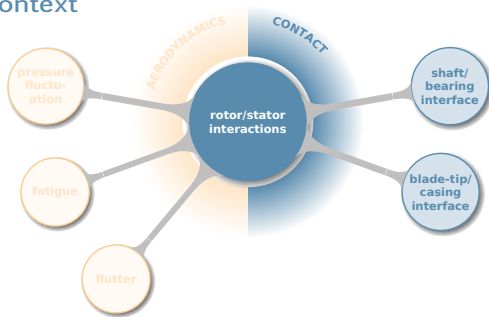
17. S. Edwards et al. en. *Journal of Sound and Vibration* (1999). doi: [10.1006/jsvi.1999.2302](https://doi.org/10.1006/jsvi.1999.2302).

18. N. Lesaffre et al. en. *European Journal of Mechanics - A/Solids* (2007). doi: [10.1016/j.euromechso1.2006.11.002](https://doi.org/10.1016/j.euromechso1.2006.11.002).

19. M. Legrand et al. en. *Journal of Sound and Vibration* (2012). doi: [10.1016/j.jsv.2012.01.017](https://doi.org/10.1016/j.jsv.2012.01.017).



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17. S. Edwards et al. en. *Journal of Sound and Vibration* (1999). doi: [10.1006/jsvi.1999.2302](https://doi.org/10.1006/jsvi.1999.2302).

18. N. Lesaffre et al. en. *European Journal of Mechanics - A/Solids* (2007). doi: [10.1016/j.euromechso1.2006.11.002](https://doi.org/10.1016/j.euromechso1.2006.11.002).

19. M. Legrand et al. en. *Journal of Sound and Vibration* (2012). doi: [10.1016/j.jsv.2012.01.017](https://doi.org/10.1016/j.jsv.2012.01.017).

I - Rotor/stator
interactions

Overview

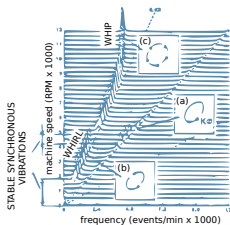
Blade/casing interface

Problem-solving
strategyII - Research
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applicationsIV - Going
forward...

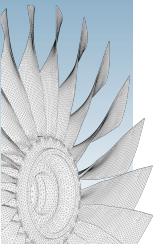
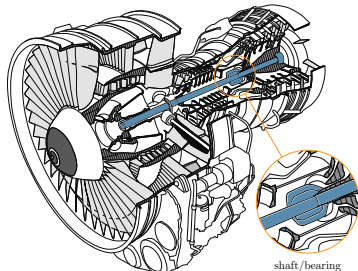
References

Shaft/bearing

- shaft orbital motions due to mass unbalance or misalignment
- contacts between shaft and supporting bearings
- modelling strategies:
 - ▶ single rotors: Black,²⁰ Jeffcott
 - ▶ dual rotors: Childs²¹



▶ waterfall diagram²²



20. H. F. Black. en. *Journal of Mechanical Engineering Science* (2006). doi: [10.1243/JMES_JOUR_1968_010_003_02](https://doi.org/10.1243/JMES_JOUR_1968_010_003_02).

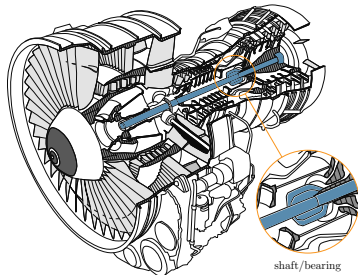
21. D. W. Childs. en. *Journal of Engineering for Industry* (1976). doi: [10.1115/1.3439046](https://doi.org/10.1115/1.3439046).

22. A. Muszynska. en. *Journal of Sound and Vibration* (1986). doi: [10.1016/S0022-460X\(86\)80146-8](https://doi.org/10.1016/S0022-460X(86)80146-8).



Shaft/bearing

- shaft orbital motions due to mass unbalance or misalignment
- contacts between shaft and supporting bearings
- modelling strategies:
 - ▶ single rotors: Black,²⁰ Jeffcott
 - ▶ dual rotors: Childs²¹
- interface characterized by:
 - ▶ non-accidental and accidental configurations
 - ▶ impacting components often considered rigid
 - ▶ small relative displacements
 - ▶ essentially structural dynamics considerations



shaft/bearing

20. H. F. Black. en. *Journal of Mechanical Engineering Science* (2006). doi: [10.1243/JMES_JOUR_1968_010_003_02](https://doi.org/10.1243/JMES_JOUR_1968_010_003_02).

21. D. W. Childs. en. *Journal of Engineering for Industry* (1976). doi: [10.1115/1.3439046](https://doi.org/10.1115/1.3439046).

22. A. Muszynska. en. *Journal of Sound and Vibration* (1986). doi: [10.1016/S0022-460X\(86\)80146-8](https://doi.org/10.1016/S0022-460X(86)80146-8).



I - Rotor/stator interactions

Overview

Blade/casing interface

Problem-solving strategy

II - Research investigations

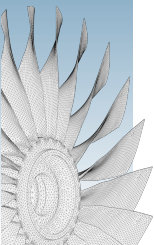
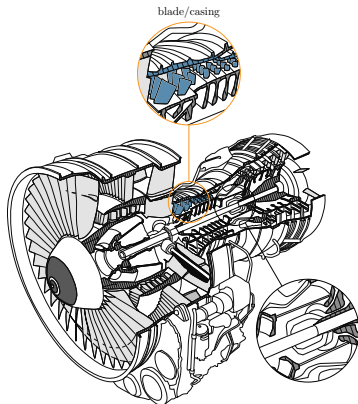
III - Industrial applications

IV - Going forward...

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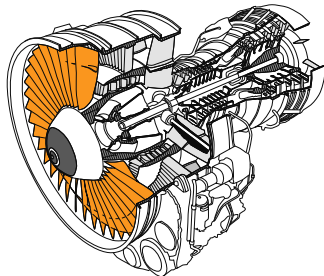
Blade/casing

- requires high resolution models for accurate results
- interface characterized by:
 - ▶ very high relative speeds (500 m/s)
 - ▶ inherently multiphysics: aerodynamic loading + blade vibrations + abrasible coating wear + thermomechanics
 - ▶ combination of several types of nonlinearities: contact + geometric (fan, turbines)
 - ▶ shift of blades' eigenfrequencies (impact on critical speeds prediction)
- influence of operating clearances on overall efficiency ⇒ **key interface for designers**
- relevant interface at **all stages of an engine**





- specificities
 - ▶ large slender blades
 - ▶ geometrical nonlinearities may be accounted for
 - ▶ use of composite materials
- modal interactions
 - ▶ blade and casing exchange energy through repeated structural contacts
 - ▶ under specific conditions, geometrical match (same nodal diameter)
- orbital motions in accidental configurations
 - ▶ bearing failure
 - ▶ forward and backward whirl motions



Interaction phenomena

- modal interaction (dynamics)^{23, 24}
- whirl motions (dynamics + inertial effects)²⁵

23. P. Schmiechen. en. PhD thesis. 1997, [available online](#).

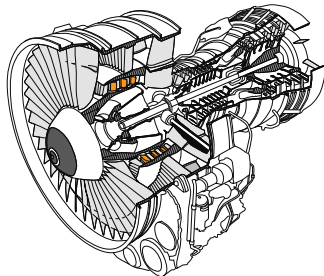
24. M. Legrand et al. en. *Journal of Sound and Vibration* (2009). doi: [10.1016/j.jsv.2008.06.019](#).

25. N. Salvat et al. en. *International Journal of Non-Linear Mechanics* (2016). doi: [10.1016/j.ijnonlinmec.2015.10.001](#).



Low-pressure compressor

- design considerations
 - ▶ operating clearances must be minimized for higher efficiency
 - ▶ high cost associated to blade maintenance
- specificities
 - ▶ frequent use of abradable coatings (AlSi-Polyester...) ²⁶
 - ▶ rigid casings and usually limited influence of disk modes ²⁷
- rubbing interactions
 - ▶ localized interaction involving a single blade ²⁸
 - ▶ sophisticated wear related physical phenomena (grooving, material transfer...)



Interaction phenomena

- rubbing (blade dynamics + wear)

26. L. T. Shiembob. Technical report. 1975, [available online](#).

27. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2015. doi: [10.1115/GT2015-42682](#).

28. K. E. Turner et al. en. American Society of Mechanical Engineers Digital Collection, 2010. doi: [10.1115/GT2010-22166](#).



High-pressure compressor

I - Rotor/stator interactions

Overview

Blade/casing interface

Problem-solving strategy

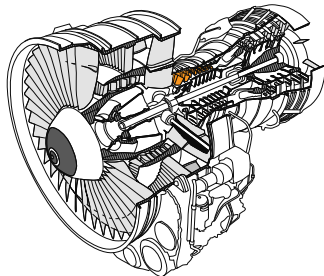
II - Research investigations

III - Industrial applications

IV - Going forward...

References

- design challenges
 - ▶ frequent use of blisks
 - ▶ disk dynamics must be considered
 - ▶ operating clearances must be minimal
- modal interactions
 - ▶ requires the modelling of the full bladed disk²⁹
 - ▶ on-going investigations with respect to inter-stage coupling³⁰
- rubbing interactions
 - ▶ localized interaction involving a single blade³¹
 - ▶ sophisticated wear related physical phenomena (grooving, material transfer...)



Interaction phenomena

- modal interaction (dynamics + wear)
- rubbing (blade dynamics + wear + thermomechanics)

29. M. Legrand et al. en. *Journal of Sound and Vibration* (2012). doi: [10.1016/j.jsv.2012.01.017](https://doi.org/10.1016/j.jsv.2012.01.017).

30. G. Battiato et al. en. *Journal of Engineering for Gas Turbines and Power* (2018). doi: [10.1115/1.4038348](https://doi.org/10.1115/1.4038348).

31. A. Batailly et al. en. *Journal of Sound and Vibration* (2016). doi: [10.1016/j.jsv.2016.03.016](https://doi.org/10.1016/j.jsv.2016.03.016).



Turbine stages

I - Rotor/stator interactions

Overview

Blade/casing interface

Problem-solving strategy

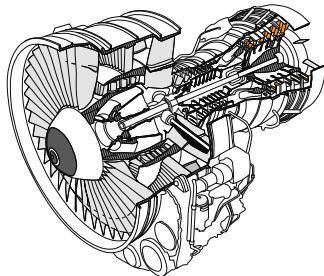
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References

- design challenges
 - ▶ use of new heat resistant CMC materials (stator shroud segments...) ³²
 - ▶ more complex blade geometries
 - ▶ use of thermally sprayed coatings on blades ³³
- specificities
 - ▶ extreme temperatures
 - ▶ non-negligible blade to blade contacts (shrouds...)
- rubbing interactions
 - ▶ localized interaction involving a single blade
 - ▶ sophisticated wear related physical phenomena (grooving, material transfer...) ³⁴



Interaction phenomena

- rubbing (blade dynamics + wear + thermomechanics)

32. F. Nyssen et al. en. *Journal of Sound and Vibration* (2020). doi: [10.1016/j.jsv.2019.115040](https://doi.org/10.1016/j.jsv.2019.115040).

33. S. Colón et al. en. American Society of Mechanical Engineers Digital Collection, 2019. doi: [10.1115/GT2019-90886](https://doi.org/10.1115/GT2019-90886).

34. R. K. Schmid. en. PhD thesis. ETH Zurich, 1997. doi: [10.3929/ethz-a-001809249](https://doi.org/10.3929/ethz-a-001809249).

Research context

Review articles in the field of rotor/stator contacts

- 1969 - shaft/bearing interface³⁵
- 1989 - shaft/bearing interface³⁶
- 2010 - shaft/bearing interface³⁷
- 2013 - blade/casing interface (mostly)³⁸
- 2016 - blade/casing interface³⁹
- 2020 - both interfaces⁴⁰

35. A. D. Dimarogonas et al. en. *Wear* (1969). doi: [10.1016/0043-1648\(69\)90037-4](https://doi.org/10.1016/0043-1648(69)90037-4).

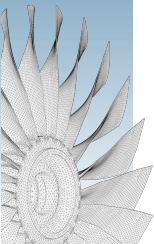
36. A. Muszynska. *Rotor-to-stationary element sub-related vibration phenomena in rotating machinery: literature survey* (1989).

37. S. Ahmad. *Journal of Vibration and Control* (2010). doi: [10.1177/1077546309341605](https://doi.org/10.1177/1077546309341605).

38. G. Jacquet-Richardet et al. en. *Mechanical Systems and Signal Processing* (2013). doi: [10.1016/j.ymssp.2013.05.010](https://doi.org/10.1016/j.ymssp.2013.05.010).

39. H. Ma et al. en. *Nonlinear Dynamics* (2016). doi: [10.1007/s11071-015-2535-x](https://doi.org/10.1007/s11071-015-2535-x).

40. K. Prabith et al. en. *Nonlinear Dynamics* (2020). doi: [10.1007/s11071-020-05832-y](https://doi.org/10.1007/s11071-020-05832-y).





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- 2020 - both interfaces⁴⁰

Purpose of this presentation

- emphasize the specificity of the blade/casing interface
- contextualize research works with respect to industrial needs
- bridge research on wear modelling and research on abrasible coatings with recent numerical developments

35. A. D. Dimarogonas et al. en. *Wear* (1969). doi: [10.1016/0043-1648\(69\)90037-4](https://doi.org/10.1016/0043-1648(69)90037-4).

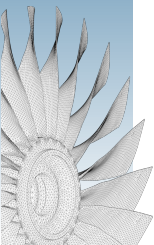
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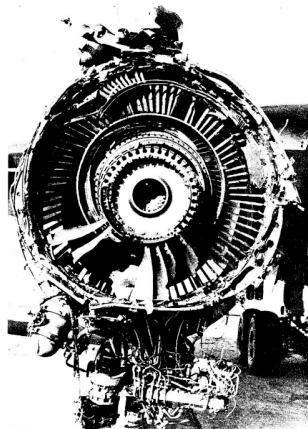




Multifaceted challenges

- aerospace industry: major safety concerns^{41, 42, 43}
- power generation: maintenance and cost issues⁴⁴
- automotive industry: mostly a performance issue

Most of the research works detailed in the remainder are related to the aerospace industry.



▶ photo from⁴¹

-
41. H. R. John et al. Technical report. National Transport Safety Board, 1975, [available online](#).
 42. C. A. Christie. Aviation Rulemaking Advisory Committee. FAA, 1996, [available online](#).
 43. Technical report. Australian Transport Safety Bureau, 2008, [available online](#).
 44. C. J. Hulme et al. en. American Society of Mechanical Engineers Digital Collection, 2015. doi: [10.1115/GT2015-43312](#).



Understanding and predicting blade/casing contacts

I - Rotor/stator interactions

Overview

Blade/casing interface

Problem-solving strategy

II - Research investigations

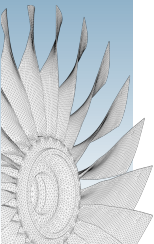
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full scale
exp. setups





Understanding and predicting blade/casing contacts

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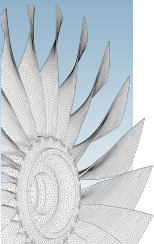
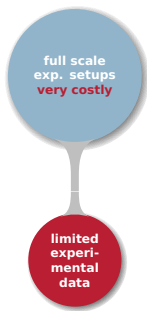
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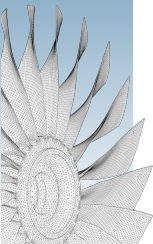
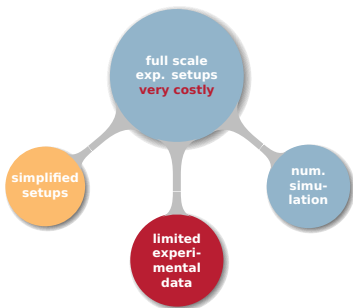
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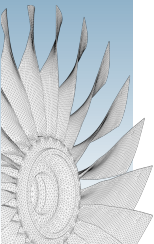
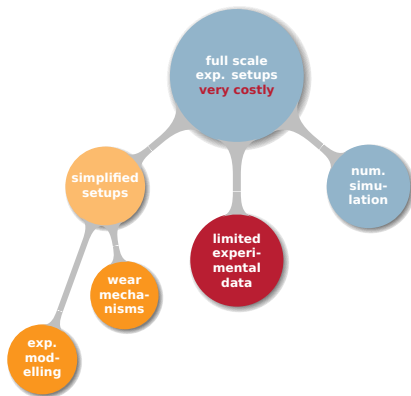
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Overview

Blade/casing interface

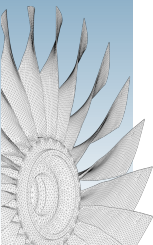
Problem-solving strategy

II - Research investigations

III - Industrial applications

IV - Going forward...

References





Understanding and predicting blade/casing contacts

I - Rotor/stator interactions

Overview

Blade/casing interface

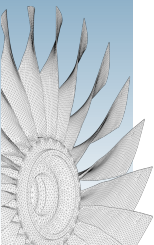
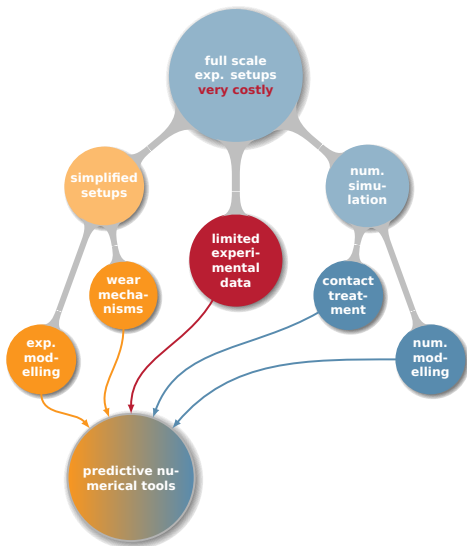
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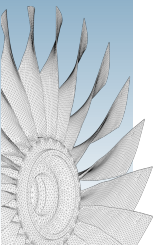
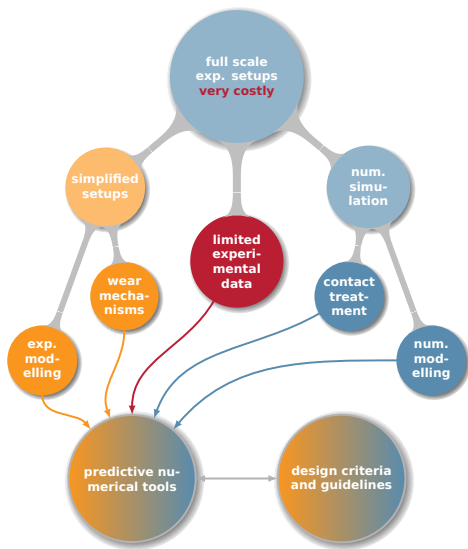
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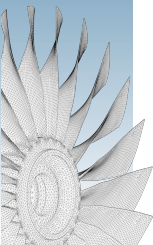
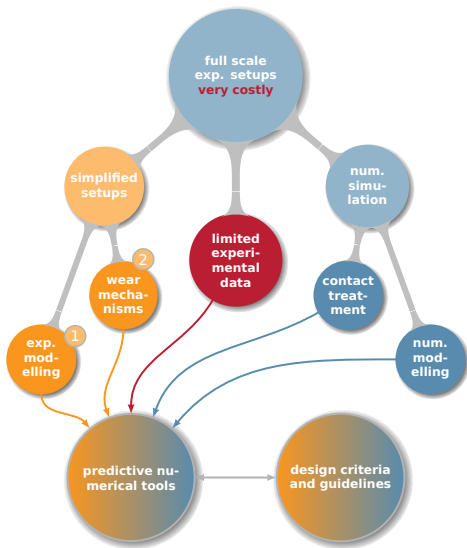
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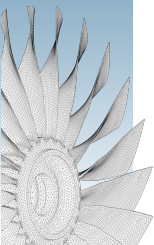
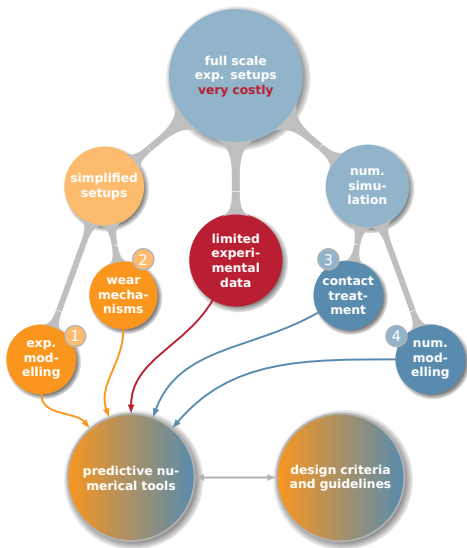
Problem-solving strategy

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IV - Going forward...

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I - Rotor/stator
interactions

**II - Research
investigations**

Material and
experimental

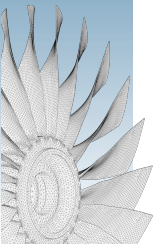
Theoretical and
numerical

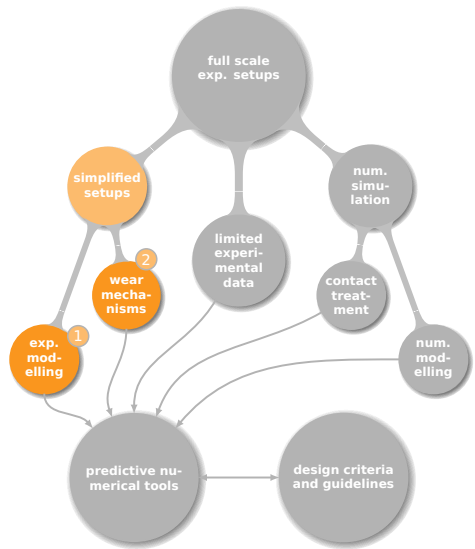
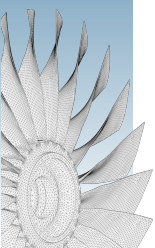
III - Industrial
applications

IV - Going
forward...

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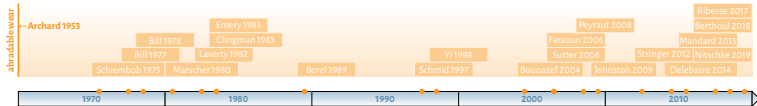
② Research investigations







Abradable coating mechanical properties



II - Research investigations

Material and experimental

Abradable coating

Simpl. exp. setups

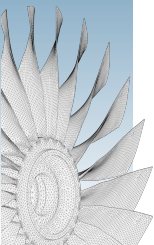
Full scale setups

Theoretical and numerical

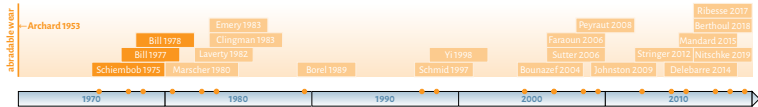
III - Industrial applications

IV - Going forward...

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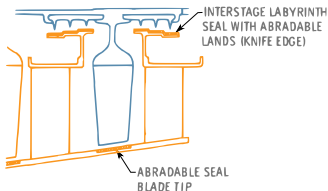


Abradable coating mechanical properties



Development of abradable materials

- knife edge seals applications⁴⁵
- various alloys and honeycomb structures
- compromise to be found between:
 - ▶ abradability of the material⁴⁶
 - ▶ erosion performance and thermal resistance

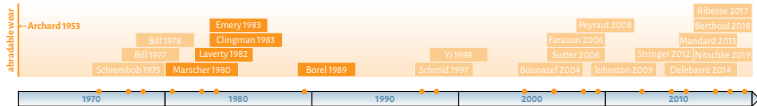


47

45. L. T. Shiembob. Technical report. 1975, available online.
 46. R. C. Bill et al. en. 1978, available online.
 47. R. C. Bill et al. en. *Journal of Lubrication Technology* (1977). doi: 10.1115/1.3453236.

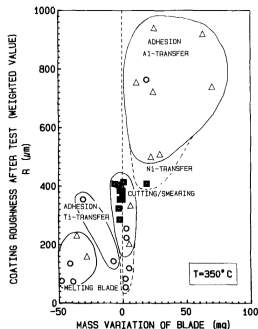


Abradable coating mechanical properties



Wear mechanisms in gas turbines

- growing interest for blade/casing contacts⁴⁸ and ceramic seals⁴⁹
- first description of wear models⁵⁰ and detailed description of thermomechanical phenomena
- description of distinct wear mechanisms in gas turbines abradable seals⁵¹



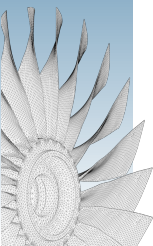
► wear mechanisms identified in⁵¹

48. A. F. Emery et al. en. *Wear* (1983). doi: [10.1016/0043-1648\(83\)90248-X](https://doi.org/10.1016/0043-1648(83)90248-X).

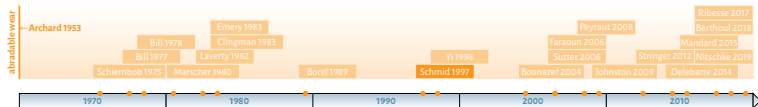
49. D. L. S. Clingman. *Lubrication Engineering* (1983, available online).

50. W. D. Marscher. en. *Wear* (1980). doi: [10.1016/0043-1648\(80\)90278-1](https://doi.org/10.1016/0043-1648(80)90278-1).

51. M. O. Borel et al. en. *Surface and Coatings Technology* (1989). doi: [10.1016/0257-8972\(89\)90046-7](https://doi.org/10.1016/0257-8972(89)90046-7).

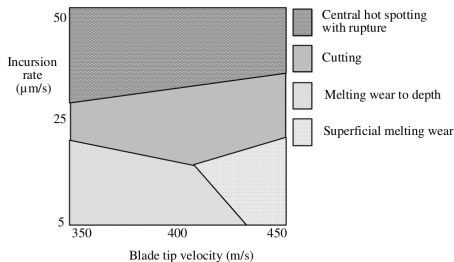


Abradable coating mechanical properties



Performance analysis of abradable seals ⁵²

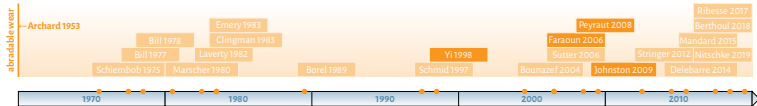
- focus on purely material aspects (no vibration aspects)
- expansion and generalization of Borel's work
- use of wear maps for performance comparisons



► wear map of AlSi abradable coatings at 400°C from ⁵²

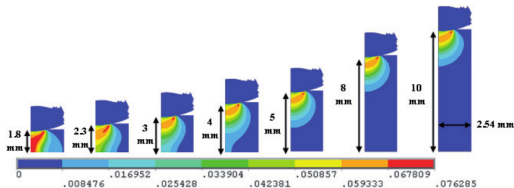


Abradable coating mechanical properties



Static / low-speed characterization of abradable seals

- use of scratch tests⁵³ and HR15Y⁵⁴
- first numerical models (static, FE) of abradable seals⁵⁵
- analysis of distinct types of wear (adhesive, abrasive, oxidation...)



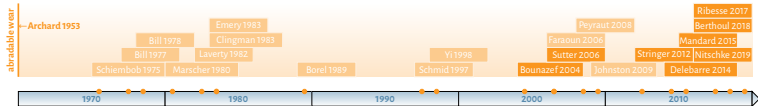
► results of finite element computations carried out in⁵⁵

54. M. Yi et al. (1998, [available online](#)).

55. F. Peyraut et al. en. *Int. J. for Simulation and Multidisciplinary Design Optimization* (2008). doi: 10.1051/ijsmdo:2008028.

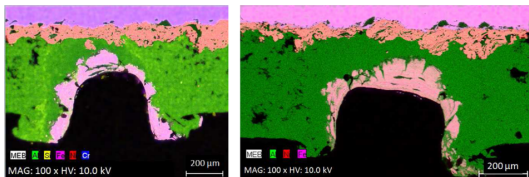
56. H. I. Faraoun et al. en. *Surface and Coatings Technology* (2006). doi: 10.1016/j.surfcoat.2005.11.105.

Abradable coating mechanical properties



Dynamic characterization, interaction with blade dynamics

- rubbing is now accepted as a non-accidental event by manufacturers⁵⁷
- growing interest for the vibration behaviour of the impacting component⁵⁸
- investigations on complex transfer phenomena⁵⁹
- more realistic experimental setups aiming at engine-like conditions⁶⁰



► Energy-dispersive X-ray spectroscopy of an abradable coating shown in⁶⁰

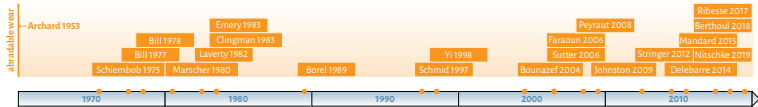
58. B. Berthoul et al. en. *Mechanical Systems and Signal Processing* (2018). doi: 10.1016/j.ymsp.2017.05.020.

59. R. Mandard et al. en. *Tribology International* (2015). doi: 10.1016/j.triboint.2014.01.026.

60. C. Delebarre et al. en. *Wear* (2014). doi: 10.1016/j.wear.2014.04.023.

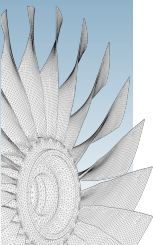
61. S. Nitschke et al. en. *Wear* (2019). doi: 10.1016/j.wear.2018.12.072.

Abradable coating mechanical properties



Over time: two types of experimental setups

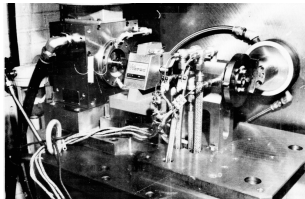
- investigating wear mechanisms (1975-today)
 - ▶ incursion rate
 - ▶ relative interaction speed
 - ▶ material type
- focusing on blade vibrations and complex chemical interactions (2000-today)
 - ▶ variation of blade profile
 - ▶ engine-like conditions



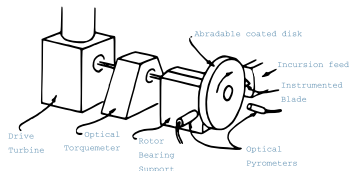


Simplified experimental setups

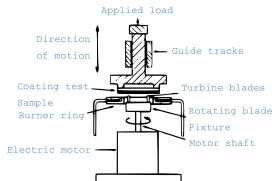
- 1975: NASA / Pratt & Whitney⁶²
 - ▶ development of abradable coatings for high temperature environments (850 - 1100°C)
 - ▶ compromise between erosion performance and abradability



- 1982: Pratt & Whitney⁶³
 - ▶ interaction with fibermetal strips
 - ▶ single blade, room temperature



- 1982: Metco⁶⁴
 - ▶ setup for ceramic abradable turbine seal
 - ▶ constant contact over time
 - ▶ heated coating (1100°C)



62. L. T. Shiembob. Technical report. 1975, available online.

63. W. F. Lavery. en. *Wear* (1982). doi: 10.1016/0043-1648(82)90137-5.

64. E. Novinski et al. en. *Thin Solid Films* (1982). doi: 10.1016/0040-6090(82)90018-9.



Simplified experimental setups

I - Rotor/stator interactions

II - Research investigations

Material and experimental

Abradable coating

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Full scale setups

Theoretical and numerical

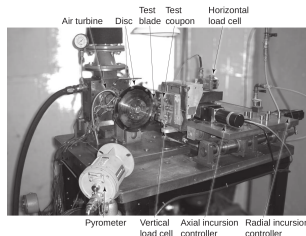
III - Industrial applications

IV - Going forward...

References

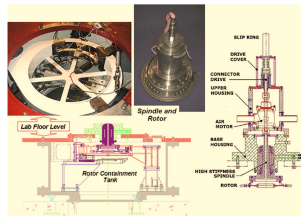
● 2008: Gas Turbine Laboratory (CNRC)⁶⁵

- ▶ effect of temperature on abradable seals
- ▶ influence of other parameters including:
 - blade rotation speed
 - incursion rate



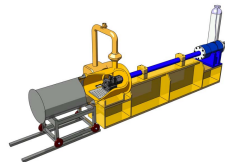
● 2002 / 2010: Gas Turbine Laboratory (OSU - GE)⁶⁶

- ▶ use of actual aircraft engine blades
- ▶ engine-like conditions (speed, contact profile)
- ▶ Rotor-Blade Rub database



● 2012: ENIM - Snecma⁶⁷

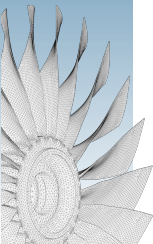
- ▶ titanium projected on an abradable layer
- ▶ focus on the measurement of cutting forces
- ▶ large incursion rates



65. A. Dadouche et al. en. American Society of Mechanical Engineers Digital Collection, 2009. doi: [10.1115/GT2008-51228](https://doi.org/10.1115/GT2008-51228).

66. C. Padova et al. en. *Journal of Turbomachinery* (2011). doi: [10.1115/1.4000539](https://doi.org/10.1115/1.4000539).

67. M. Cuny et al. en. *Experimental Mechanics* (2014). doi: [10.1007/s11340-013-9780-z](https://doi.org/10.1007/s11340-013-9780-z).

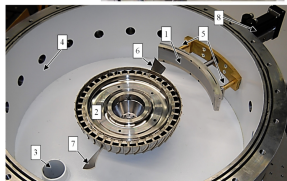
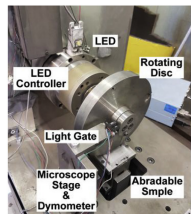
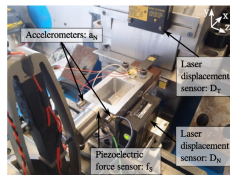


Simplified experimental setups

- 2015: ONERA - Snecma⁶⁸
 - ▶ rectangular plate / coated cylinder
 - ▶ focus on the blade vibrations

- 2018: University of Sheffield⁶⁹
 - ▶ small simplified blades
 - ▶ variation of wear processes with time

- 2019: Technische Universität Dresden - Rolls-Royce⁷⁰
 - ▶ use of actual aircraft engine blades
 - ▶ multiple impacts per revolution are possible
 - ▶ engine-like boundary conditions



- 1: 72° casing segment with abradable liner material
- 2: bladed disk mounted on spindle drive
- 3: vacuum access
- 4: steel containment
- 5: linear guidance
- 6: test blade
- 7: counter blade
- 8: linear feed motor for axial movement of the casing segment

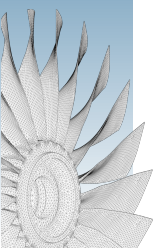
68. R. Mandard et al. en. *Tribology International* (2015). doi: [10.1016/j.triboint.2014.01.026](https://doi.org/10.1016/j.triboint.2014.01.026).

69. B. Zhang et al. en. *Wear* (2019). doi: [10.1016/j.wear.2019.01.034](https://doi.org/10.1016/j.wear.2019.01.034).

70. S. Nitschke et al. en. *Wear* (2019). doi: [10.1016/j.wear.2018.12.072](https://doi.org/10.1016/j.wear.2018.12.072).

Simplified experimental setups

- 1978: Lewis Research Center (NASA)⁷¹
- 2002: Central South University of Technology⁷²
- 2004: UTBM⁷³
- 2007: Alstom⁷⁴
- 2014: ENIT - Snecma⁷⁵
 - ▶ focus on labyrinth seals
 - ▶ investigations on material transfer



71. R. C. Bill et al. en. 1978, [available online](#).

72. Y. Maozhong et al. en. *Wear* (2002). doi: [10.1016/S0043-1648\(01\)00681-0](#).

73. M. Bounazef et al. en. *Materials Letters* (2004). doi: [10.1016/j.matlet.2004.02.049](#).

74. U. Rathmann et al. en. American Society of Mechanical Engineers Digital Collection, 2009. doi: [10.1115/GT2007-27724](#).

75. C. Delebarre et al. en. *Wear* (2014). doi: [10.1016/j.wear.2014.04.023](#).



I - Rotor/stator interactions

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Material and experimental

Abradable coating

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Full scale setups

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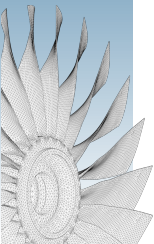
III - Industrial applications

IV - Going forward...

References

Summary of experimental investigations

- 1975-2020: from coating investigations to the characterization of lighter materials (CMC turbine shrouds⁷⁶)
 - ▶ initial focus on abradable coating mechanical properties in a context where contacts were accidental
 - ▶ growing interest for the influence of contacts on the blade response
 - ▶ integration of contacts within design certification process





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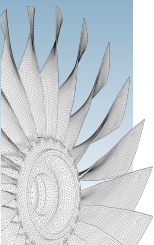
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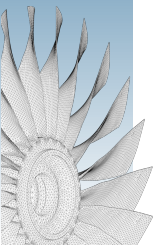
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 - ▶ initial focus on abradable coating mechanical properties in a context where contacts were accidental
 - ▶ growing interest for the influence of contacts on the blade response
 - ▶ integration of contacts within design certification process
- abradable coatings can now be used in every stage of a turbomachine
- which yields higher efficiency (gas turbines and aircraft engines)
- variety of technological solutions available (AlSi-Polyester, ceramic, honeycomb)...
- ...that requires stage by stage analyses of rubbing interactions...
- and motivates the development of realistic setups featuring actual blades and interchangeable abradable samples



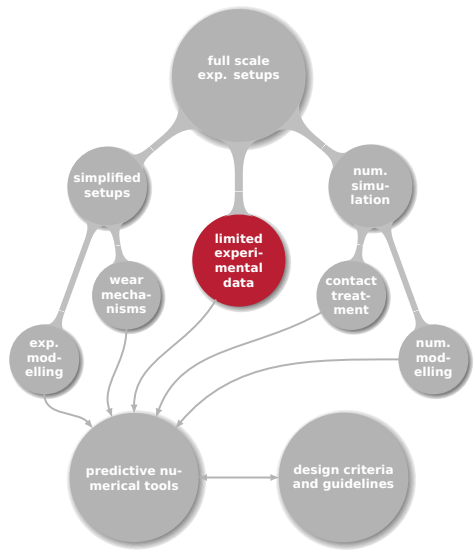
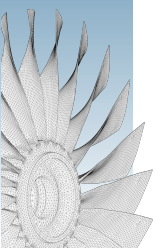
Challenges and open research questions

- many wear mechanisms are still not fully understood
 - ▶ material transfer (blade on casing or casing on blade)
 - ▶ grooving phenomena in the abradable seal
- specific challenges in turbine stages where blades feature protective coatings⁷⁷
- mechanical characterization of abradable coatings (modelling) is an open question⁷⁸



77. S. Colón et al. en. American Society of Mechanical Engineers Digital Collection, 2019. doi: [10.1115/GT2019-90886](https://doi.org/10.1115/GT2019-90886).

78. S. Skiba et al. en. *Journal of Dynamic Behavior of Materials* (2020). doi: [10.1007/s40870-020-00242-y](https://doi.org/10.1007/s40870-020-00242-y).





Full-scale experimental setups

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- no existing facility for multi-stage full-scale experimental setups
- existing experimental setups feature a **single** stage
- most investigations are carried out under vacuum
 - ▶ rubbing interaction within low-pressure compressor⁷⁹
 - ▶ rubbing interaction within high-pressure compressor⁸⁰
 - ▶ Large Spin Pit Facility (LSPF) at OSU⁸¹
 - ▶ PHARE experimental setup in ECL⁸²



picture of the Equipex-PHARE test bench (source)

79. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2010. doi: [10.1115/DETC2009-86842](https://doi.org/10.1115/DETC2009-86842).

80. A. Batailly et al. en. *Journal of Sound and Vibration* (2016). doi: [10.1016/j.jsv.2016.03.016](https://doi.org/10.1016/j.jsv.2016.03.016).

81. N. Langenbrunner et al. en. *Journal of Engineering for Gas Turbines and Power* (2015). doi: [10.1115/1.4028685](https://doi.org/10.1115/1.4028685).

82. F. Thouverez. fr. PHARE Plateforme machines tournantes pour la maîtrise des Risques Environnementaux (). doi: <https://www.ec-lyon.fr/campus/vie-campus/grands-projets/equipex-phare>.



I - Rotor/stator
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Solution strategy

Contact mechanics

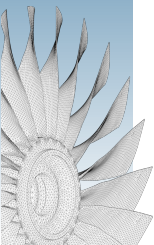
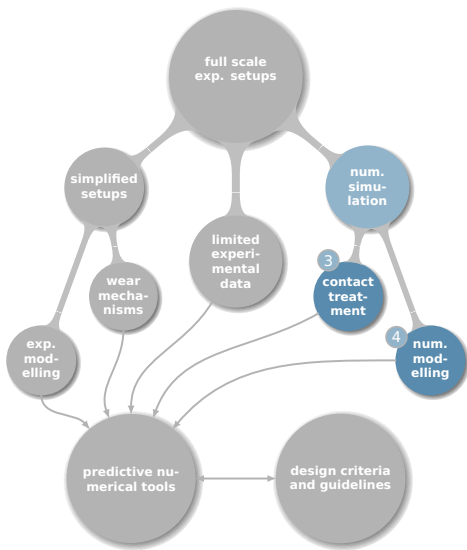
Model reduction

Multiphysics

III - Industrial
applications

IV - Going
forward...

References





Numerical framework

Each type of blade/casing interaction requires a specific numerical framework:

rotor	stator	interactions	required features
1 blade	rigid (flexible)	rubbing	contact treatment
			structural dynamics
			wear
full bladed disk	flexible	modal interaction	contact treatment
			structural dynamics
			two flexible components
bladed disk + shaft	flexible (rigid)	whirl motions	contact treatment
			structural dynamics
			inertial effects

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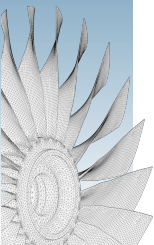
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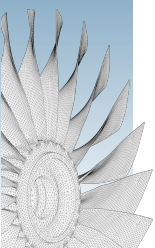
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1 blade	rigid (flexible)	rubbing	contact treatment structural dynamics wear
full bladed disk	flexible	modal interaction	contact treatment structural dynamics two flexible components
bladed disk + shaft	flexible (rigid)	whirl motions	contact treatment structural dynamics inertial effects

Modal interaction

- full bladed disk required
- both stator and rotor must be flexible⁸³
- significant computational cost \Rightarrow use of phenomenological models⁸⁴

83. P. Schmiechen. en. PhD thesis. 1997, [available online](#).

84. M. Legrand et al. en. *Journal of Sound and Vibration* (2009). doi: [10.1016/j.jsv.2008.06.019](https://doi.org/10.1016/j.jsv.2008.06.019).



Numerical framework

Each type of blade/casing interaction requires a specific numerical framework:

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			structural dynamics
			wear
full bladed disk	flexible	modal interaction	contact treatment
			structural dynamics
			two flexible components
bladed disk + shaft	flexible (rigid)	whirl motions	contact treatment
			structural dynamics
			inertial effects

Rubbing

- very precise modelling of the blade/casing interface is required⁸⁵
- live update of clearances due to wear is key^{86, 87}
- industrial 3D finite element models are usually considered⁸⁸

85. M. Legrand et al. en. *Journal of Sound and Vibration* (2012). doi: [10.1016/j.jsv.2012.01.017](https://doi.org/10.1016/j.jsv.2012.01.017).

86. M. Legrand et al. en. American Society of Mechanical Engineers Digital Collection, 2010. doi: [10.1115/DETC2009-87669](https://doi.org/10.1115/DETC2009-87669).

87. R. J. Williams. en. American Society of Mechanical Engineers Digital Collection, 2012. doi: [10.1115/GT2011-45495](https://doi.org/10.1115/GT2011-45495).

88. A. Batailly et al. en. *Journal of Engineering for Gas Turbines and Power* (2012). doi: [10.1115/1.4006446](https://doi.org/10.1115/1.4006446).



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bladed disk + shaft	flexible (rigid)	whirl motions	contact treatment structural dynamics inertial effects

Whirl motions

- inertial effects cannot be neglected due to orbital motions
- both phenomenological⁸⁹ and full FE⁹⁰ models are considered
- published data for such interactions are very scarce

89. M.-O. Parent et al. en. American Society of Mechanical Engineers Digital Collection, 2014. doi: [10.1115/GT2014-25253](https://doi.org/10.1115/GT2014-25253).

90. N. Salvat et al. en. *International Journal of Non-Linear Mechanics* (2016). doi: [10.1016/j.ijnonlinmec.2015.10.001](https://doi.org/10.1016/j.ijnonlinmec.2015.10.001).



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			inertial effects

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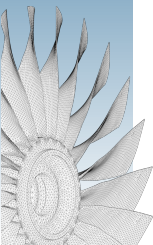
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bladed disk + shaft	flexible (rigid)	whirl motions	contact treatment
			structural dynamics
			inertial effects

Numerical and theoretical challenges

1 solution strategy

- ▶ periodic (synchronous) motions can reasonably be expected in aircraft engines...
- ▶ ...but transient phenomena seem key for the rise of critical interactions⁹¹
- ▶ two types of strategies: frequency methods^{92, 93} vs. time integration⁹⁴

2 contact mechanics

3 modelling

91. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2010. doi: [10.1115/DETC2009-86842](https://doi.org/10.1115/DETC2009-86842).

92. G. von Groll et al. en. *Journal of Sound and Vibration* (2001). doi: [10.1006/jsvi.2000.3298](https://doi.org/10.1006/jsvi.2000.3298).

93. L. Salles et al. en. American Society of Mechanical Engineers Digital Collection, 2010. doi: [10.1115/GT2010-23264](https://doi.org/10.1115/GT2010-23264).

94. N. J. Carpenter et al. en. *International Journal for Numerical Methods in Engineering* (1991). doi: [10.1002/nme.1620320107](https://doi.org/10.1002/nme.1620320107). 51/97



Numerical framework

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bladed disk + shaft	flexible (rigid)	whirl motions	contact treatment structural dynamics inertial effects

Numerical and theoretical challenges

- ① solution strategy
- ② contact mechanics
 - ▶ inherently nonlinear mechanical system \Rightarrow **no unified theoretical framework**⁹⁵
 - ▶ numerical management of non-smooth contact algorithms yields distinct *ad hoc* strategies^{96, 97}
 - ▶ severe bottleneck for industry-ready analyses⁹⁸

95. S. K. Sinha. en. *International Journal of Non-Linear Mechanics* (2005). doi: [10.1016/j.ijnonlinmec.2004.05.019](https://doi.org/10.1016/j.ijnonlinmec.2004.05.019).

96. C. Yoong et al. en. *Nonlinear Dynamics* (2018). doi: [10.1007/s11071-017-4025-9](https://doi.org/10.1007/s11071-017-4025-9).

97. N. Lesaffre et al. en. *European Journal of Mechanics - A/Solids* (2007). doi: [10.1016/j.euromechsol.2006.11.002](https://doi.org/10.1016/j.euromechsol.2006.11.002).

98. A. Batailly et al. en. *Journal of Engineering for Gas Turbines and Power* (2015). doi: [10.1115/1.4028263](https://doi.org/10.1115/1.4028263).



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bladed disk + shaft	flexible (rigid)	whirl motions	contact treatment structural dynamics inertial effects

Numerical and theoretical challenges

- ① solution strategy
- ② contact mechanics
- ③ modelling
 - ▶ high definition finite element models are required (several millions of dof)⁹⁹
 - ▶ models must include one (or more) nonlinear interfaces¹⁰⁰
 - ▶ possible geometric nonlinearities which yield additional computational cost¹⁰¹
 - ▶ sensitivity of the results design parameters¹⁰² (mistuning...)

99. E. P. Petrov. en. American Society of Mechanical Engineers Digital Collection, 2013. doi: [10.1115/GT2012-68474](https://doi.org/10.1115/GT2012-68474).

100. E. P. Petrov. en. American Society of Mechanical Engineers Digital Collection, 2008. doi: [10.1115/GT2004-53894](https://doi.org/10.1115/GT2004-53894).

101. M. Balmaseda et al. en. American Society of Mechanical Engineers Digital Collection, 2019. doi: [10.1115/GT2019-90813](https://doi.org/10.1115/GT2019-90813).

102. A. M. Panunzio et al. en. American Society of Mechanical Engineers Digital Collection, 2015. doi: [10.1115/GT2015-43560](https://doi.org/10.1115/GT2015-43560).



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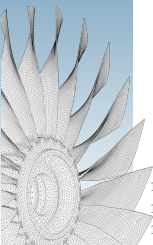
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Solution strategy

Context

- the design of mechanical systems with joint interfaces, friction or structural contacts is today a major challenge for engineers and researchers
- lack of theoretical framework (no equivalent of modal analysis in a nonlinear context)
- design relevant quantities (eigenfrequencies, mode shapes) are dependent on the amount of energy within the system
- vast amount of theoretical research work in this area:
 - ▶ nonlinear normal modes^{103, 104}
 - ▶ nonsmooth modal analysis¹⁰⁵

Specificity of the blade/casing interface

- synchronous excitation
- very small incursion rates
- inherently multi-physical
- very high relative speeds

103. G. Kerschen et al. en. *Mechanical Systems and Signal Processing* (2009). doi: [10.1016/j.ymssp.2008.04.002](https://doi.org/10.1016/j.ymssp.2008.04.002).

104. M. Krack. en. *Computers & Structures* (2015). doi: [10.1016/j.compstruc.2015.03.008](https://doi.org/10.1016/j.compstruc.2015.03.008).

105. A. Thorin et al. *SIAM Journal on Applied Dynamical Systems* (2017). doi: [10.1137/16M1081506](https://doi.org/10.1137/16M1081506).



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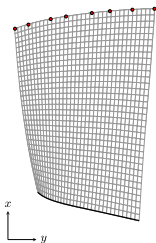
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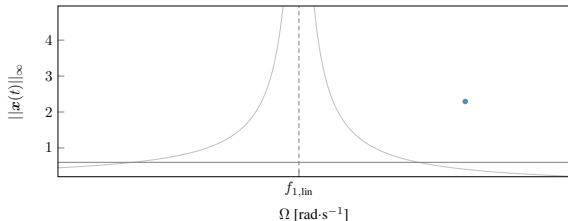
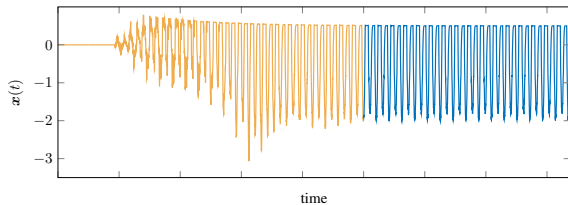
References

Two paradigms

- time integration based methods
- frequency methods



one angular speed:





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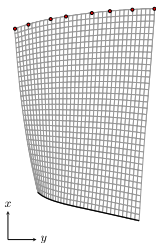
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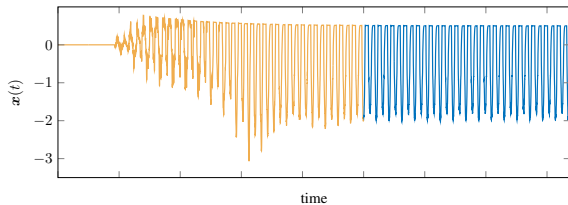
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Two paradigms

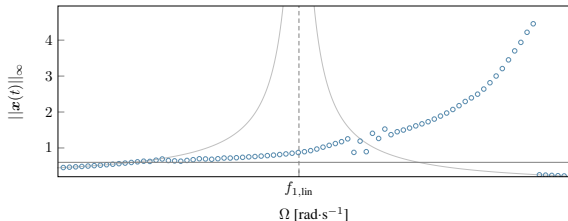
- time integration based methods
- frequency methods



one angular speed:



several angular speeds (sequential continuation $\Omega \nearrow$):





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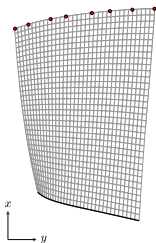
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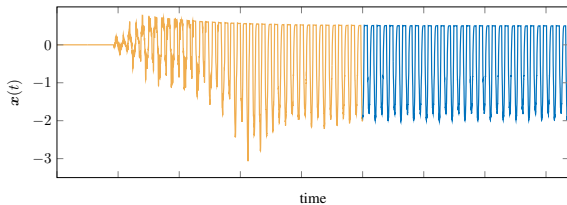
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Two paradigms

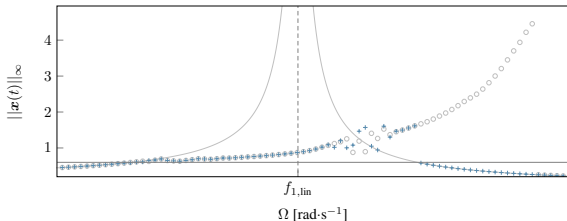
- time integration based methods
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several angular speeds (sequential continuation $\Omega \searrow$):





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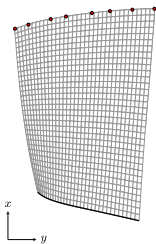
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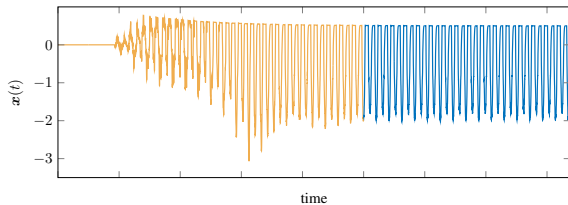
References

Two paradigms

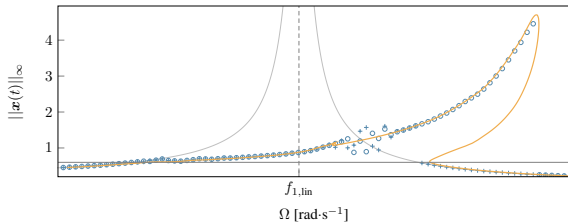
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one angular speed:



harmonic balance method (arc-length continuation):





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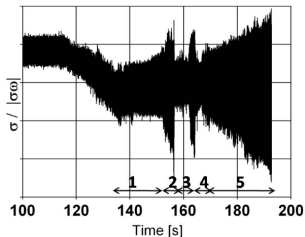
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References

Time integration methods

- experimental observations of transient phenomena and diverging interactions¹⁰⁶ have motivated the use of time integration
- both implicit¹⁰⁷ and explicit¹⁰⁸ time marching algorithms have been employed...
- ...with a variety of contact algorithms^{109, 110}



- stress signal within a blade during an interaction (Ω constant for $t > 140$ s)¹⁰⁶

106. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2010. doi: [10.1115/DETC2009-86842](https://doi.org/10.1115/DETC2009-86842).

107. L. Papeleux. 2020, [METAFOR website](#).

108. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2015. doi: [10.1115/GT2015-42682](https://doi.org/10.1115/GT2015-42682).

109. N. J. Carpenter et al. en. *International Journal for Numerical Methods in Engineering* (1991). doi: [10.1002/nme.1620320107](https://doi.org/10.1002/nme.1620320107).

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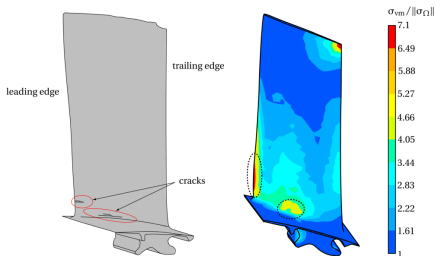
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Time integration methods

- multiple confrontations of numerical predictions with experimental results:
 - low-pressure compressor^{111, 112}
 - high-pressure compressor¹¹³
 - turbine stages¹¹⁴
- results provide a quantitative view of the problem



► experimental and numerical results shown in¹¹¹: stresses in rotor

111. A. Batailly et al. en. *Journal of Engineering for Gas Turbines and Power* (2012). doi: [10.1115/1.4006446](https://doi.org/10.1115/1.4006446).

112. Q. Agrapart et al. en. *Journal of Sound and Vibration* (2019). doi: [10.1016/j.jsv.2019.114869](https://doi.org/10.1016/j.jsv.2019.114869).

113. A. Batailly et al. en. *Journal of Sound and Vibration* (2016). doi: [10.1016/j.jsv.2016.03.016](https://doi.org/10.1016/j.jsv.2016.03.016).

114. F. Nyssen et al. en. *Journal of Sound and Vibration* (2020). doi: [10.1016/j.jsv.2019.115040](https://doi.org/10.1016/j.jsv.2019.115040).

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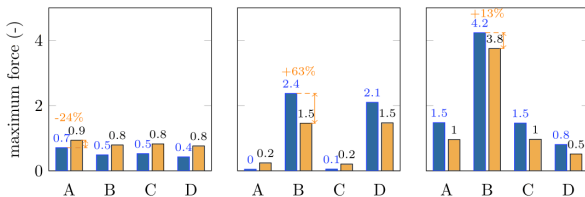
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112. Q. Agrapart et al. en. *Journal of Sound and Vibration* (2019). doi: 10.1016/j.jsv.2019.114869.

113. A. Batailly et al. en. *Journal of Sound and Vibration* (2016). doi: 10.1016/j.jsv.2016.03.016.

114. F. Nyssen et al. en. *Journal of Sound and Vibration* (2020). doi: 10.1016/j.jsv.2019.115040.



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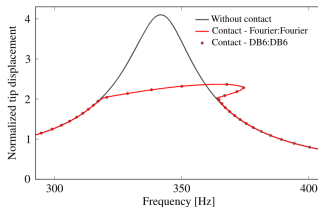
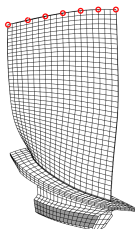
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Frequency methods

- usual numerical methodologies for shaft/bearing contacts ¹¹⁵
- structural contacts between rotor and stator yield a synchronous excitation ¹¹⁶
- many research works dedicated to the Harmonic Balance Method (HBM): multiharmonic analysis, ¹¹⁷ quasi-periodic HBM, ¹¹⁸ wavelet-based HBM ¹¹⁹ ...
- special interest for HBM in turbomachinery (HBM Tutorial ASME Turbo Expo 2018 ¹²⁰)



► model and results from ¹¹⁹: finite element mesh and frequency response function of the system

115. G. von Groll et al. en. *Journal of Sound and Vibration* (2001). doi: [10.1006/jsvi.2000.3298](https://doi.org/10.1006/jsvi.2000.3298).

116. H. Ma et al. en. *Journal of Sound and Vibration* (2015). doi: [10.1016/j.jsv.2014.10.020](https://doi.org/10.1016/j.jsv.2014.10.020).

117. E. P. Petrov. en. American Society of Mechanical Engineers Digital Collection, 2013. doi: [10.1115/GT2012-68474](https://doi.org/10.1115/GT2012-68474).

118. L. Peletan et al. en. *Nonlinear Dynamics* (2014). doi: [10.1007/s11071-014-1606-8](https://doi.org/10.1007/s11071-014-1606-8).

119. S. Jones et al. en. *International Journal for Numerical Methods in Engineering* (2015). doi: [10.1002/nme.4807](https://doi.org/10.1002/nme.4807).

120. M. Krack et al. en. American Society of Mechanical Engineers Digital Collection, 2018.



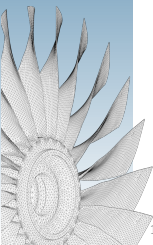
Solution strategy

Time integration

- + easy to implement and wide compatibility with contact algorithms
- + easy extension to multiphysics
- + any type of response may be computed (diverging, chaotic¹²¹...) as well as transient
- + validation by confrontation to experimental results
- results dependent on initial conditions
- a qualitative understanding of the system has a very high computational cost

Frequency methods

- + provides a qualitative understanding of the system
- + easily allows to assess the stability of a solution
- + prediction of hazardous bifurcations and multiple stable branches of solutions
- + computationally efficient but...
- ...fairly difficult to implement and CPU times explode with the number of nonlinear dof
- Fourier based analyses are sensitive to the Gibbs phenomenon





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Time integration

- variable-order fractional operators offer promising avenues for faster computations¹²²
- new contact treatment algorithms to prevent numerical artifacts¹²³
- accounting for stochastic components: mistuning¹²⁴

Frequency methods

- development of new algorithms to better handle contact nonlinearities (nonsmooth)
- path-following¹²⁵ and continuation¹²⁶ techniques
- accounting for stochastic components: uncertain nonlinear normal modes¹²⁷ and mistuning¹²⁸

122. S. Patnaik et al. en. American Society of Mechanical Engineers Digital Collection, 2019. doi: [10.1115/DETC2019-97944](https://doi.org/10.1115/DETC2019-97944).

123. A. Thorin et al. en. *Journal of Engineering for Gas Turbines and Power* (2019). doi: [10.1115/1.4040857](https://doi.org/10.1115/1.4040857).

124. J. Joachim et al. en. *Journal of Engineering for Gas Turbines and Power* (2020). doi: [10.1115/1.4047780](https://doi.org/10.1115/1.4047780).

125. A. Simon Chong Escobar et al. en. *Journal of Computational and Nonlinear Dynamics* (2017). doi: [10.1115/1.4036114](https://doi.org/10.1115/1.4036114).

126. L. Salles et al. en. *Nonlinear Dynamics* (2016). doi: [10.1007/s11071-016-3003-y](https://doi.org/10.1007/s11071-016-3003-y).

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128. C. Joannin et al. en. *Journal of Engineering for Gas Turbines and Power* (2016). doi: [10.1115/1.4031886](https://doi.org/10.1115/1.4031886).



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Solution strategy: research directions

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Frequency methods

- development of new algorithms to better handle contact nonlinearities (nonsmooth)
- path-following¹²⁵ and continuation¹²⁶ techniques
- accounting for stochastic components: uncertain nonlinear normal modes¹²⁷ and mistuning¹²⁸

Both strategies are required: time integration does not provide the required qualitative understanding of the system and frequency methods are currently not compatible with large numerical models and do not capture transient phenomena.

122. S. Patnaik et al. en. American Society of Mechanical Engineers Digital Collection, 2019. doi: [10.1115/DETC2019-97944](https://doi.org/10.1115/DETC2019-97944).

123. A. Thorin et al. en. *Journal of Engineering for Gas Turbines and Power* (2019). doi: [10.1115/1.4040857](https://doi.org/10.1115/1.4040857).

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126. L. Salles et al. en. *Nonlinear Dynamics* (2016). doi: [10.1007/s11071-016-3003-y](https://doi.org/10.1007/s11071-016-3003-y).

127. A. M. Panunzio et al. en. American Society of Mechanical Engineers Digital Collection, 2015. doi: [10.1115/GT2015-43560](https://doi.org/10.1115/GT2015-43560).

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Contact mechanics

Principle

- numerical management of unilateral contact constraints (with or without friction) remains a very active field of research¹²⁹
- contact implies both discontinuous...
 - ▶ ...velocity¹³⁰ and...
 - ▶ ...acceleration fields
- a mechanical system with contact interfaces is inherently nonlinear
 - ▶ it is difficult to accurately predict its eigenfrequencies¹³¹
 - ▶ uncertainty on the system's life span¹³²

Specificity of blade/casing interface

- very high relative speeds (500 m/s)
- very small incursion depth
- use of industrial finite elements (quadratic elements)

129. A. Thorin et al. en. *Journal of Engineering for Gas Turbines and Power* (2019). doi: [10.1115/1.4040857](https://doi.org/10.1115/1.4040857).

130. M. B. Meingast et al. en. *International Journal of Non-Linear Mechanics* (2014). doi: [10.1016/j.ijnonlinmec.2014.01.007](https://doi.org/10.1016/j.ijnonlinmec.2014.01.007).

131. D. Laxalde et al. en. *Computational Mechanics* (2011). doi: [10.1007/s00466-010-0556-3](https://doi.org/10.1007/s00466-010-0556-3).

132. W. Feifei et al. en. *Procedia Engineering* (2015). doi: [10.1016/j.proeng.2014.12.661](https://doi.org/10.1016/j.proeng.2014.12.661).



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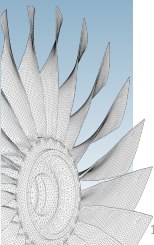
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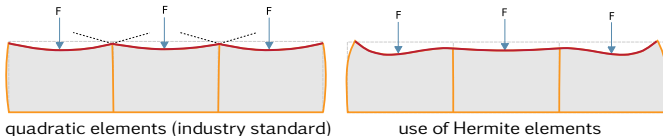
- the suitability of finite element models for contact analyses is questioned¹³³
- solving a contact problem involves the computation of two key quantities:
 - ▶ the **gap** (blade/casing clearance)
 - ▶ **contact forces**





Solution algorithms

- **gap:** a node-to-surface strategy is usually employed¹³⁴
 - ▶ quadratic FE on the casing typically yields a discontinuous normal direction to the contact surface
 - ▶ smoothing techniques are thus required for flexible casings



- ▶ challenge: compatibility with industrial procedures
- ▶ Hermite or mortar elements (mesh modification)¹³⁵
- ▶ use of non-intrusive B-splines or NURBS¹³⁶
- ▶ isogeometric analysis¹³⁷

⇒ significant numerical cost but robust procedures and industry ready solutions are available

134. P. Wriggers. en. 2nd edition. Berlin Heidelberg: Springer-Verlag, 2006. doi: [10.1007/978-3-540-32609-0](https://doi.org/10.1007/978-3-540-32609-0).

135. K. A. Fischer et al. en. *Computer Methods in Applied Mechanics and Engineering* (2006). doi: [10.1016/j.cma.2005.09.025](https://doi.org/10.1016/j.cma.2005.09.025).

136. T. Belytschko et al. en. *International Journal for Numerical Methods in Engineering* (2002). doi: [10.1002/nme.568](https://doi.org/10.1002/nme.568).

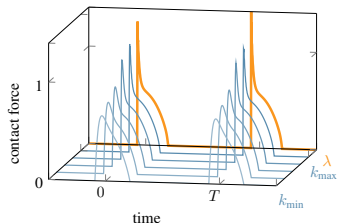
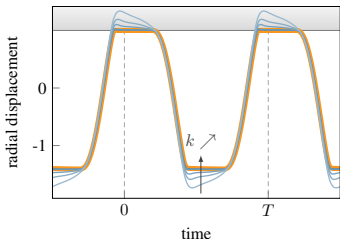
137. T. J. R. Hughes et al. en. *Computer Methods in Applied Mechanics and Engineering* (2005). doi: [10.1016/j.cma.2004.10.006](https://doi.org/10.1016/j.cma.2004.10.006)



Solution algorithms

- contact forces:

- ▶ penalty method, numerical parameter k ¹³⁸
- ▶ Lagrange multiplier-based approaches ¹³⁹



- 1-dof system with rigid impacted surface: $k \nearrow \lambda$
- numerical sensitivity increases with $k \Rightarrow$ need for smaller time steps
- k is often times used as a representation of casing stiffness ¹⁴⁰
- Lagrange multipliers-based strategies inherently forbid penetrations
- numerical artefacts on contact forces with Lagrange multipliers (initial impulsion = $f(\delta t)$)

138. H. Ma et al. en. *Journal of Sound and Vibration* (2015). doi: 10.1016/j.jsv.2014.10.020.

139. N. J. Carpenter et al. en. *International Journal for Numerical Methods in Engineering* (1991). doi: 10.1002/nme.1620320107.

140. H. Ma et al. en. *Journal of Vibration and Control* (2015). doi: 10.1177/1077546315575835.

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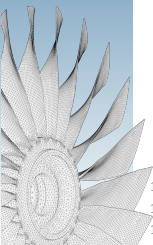
● contact forces:

- ▶ **penalty method**, numerical parameter k
- ▶ **Lagrange multiplier**-based approaches¹⁴¹
- ▶ **θ -method**¹⁴²
- ▶ **linear complementarity problem formulation**¹⁴³
- ▶ ...

141. N. J. Carpenter et al. en. *International Journal for Numerical Methods in Engineering* (1991). doi: [10.1002/nme.1620320107](https://doi.org/10.1002/nme.1620320107).

142. A. Thorin et al. en. *Journal of Engineering for Gas Turbines and Power* (2019). doi: [10.1115/1.4040857](https://doi.org/10.1115/1.4040857).

143. M. B. Meingast et al. en. *International Journal of Non-Linear Mechanics* (2014). doi: [10.1016/j.ijnonlinmec.2014.01.007](https://doi.org/10.1016/j.ijnonlinmec.2014.01.007). 65/97



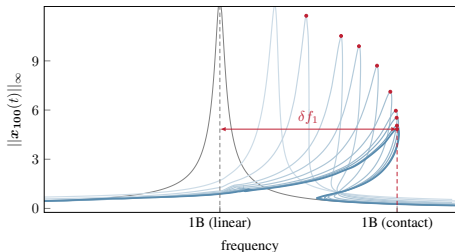


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Solution algorithms

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- ▶ penalty method, numerical parameter k
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- ▶ ...
- ▶ critical issue for design purposes: modelling of contact stiffening



141. N. J. Carpenter et al. en. *International Journal for Numerical Methods in Engineering* (1991). doi: [10.1002/nme.1620320107](https://doi.org/10.1002/nme.1620320107).

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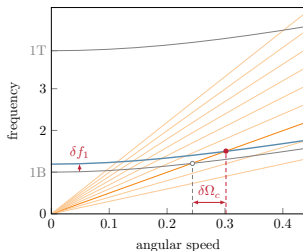
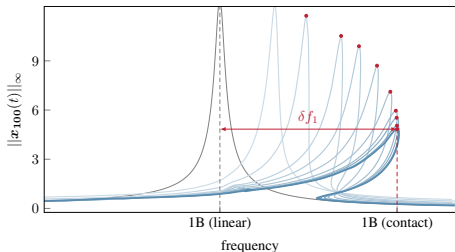
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142. A. Thorin et al. en. *Journal of Engineering for Gas Turbines and Power* (2019). doi: [10.1115/1.4040857](https://doi.org/10.1115/1.4040857).

143. M. B. Meingast et al. en. *International Journal of Non-Linear Mechanics* (2014). doi: [10.1016/j.ijnonlinmec.2014.01.007](https://doi.org/10.1016/j.ijnonlinmec.2014.01.007). 66/97

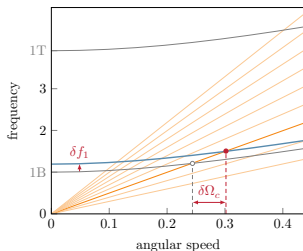
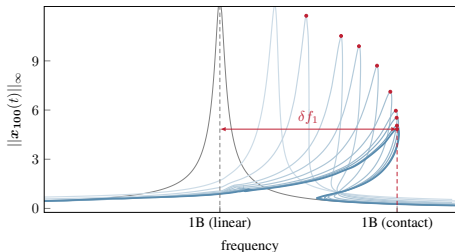


Contact mechanics

Solution algorithms

● contact forces:

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- ▶ ...
- ▶ critical issue for design purposes: modelling of contact stiffening



⇒ significant impact on the prediction of critical speeds

141. N. J. Carpenter et al. en. *International Journal for Numerical Methods in Engineering* (1991). doi: [10.1002/nme.1620320107](https://doi.org/10.1002/nme.1620320107).

142. A. Thorin et al. en. *Journal of Engineering for Gas Turbines and Power* (2019). doi: [10.1115/1.4040857](https://doi.org/10.1115/1.4040857).

143. M. B. Meingast et al. en. *International Journal of Non-Linear Mechanics* (2014). doi: [10.1016/j.ijnonlinmec.2014.01.007](https://doi.org/10.1016/j.ijnonlinmec.2014.01.007). 66/97



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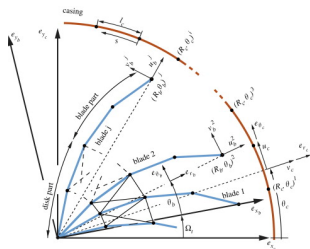
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Types of models

- analytical models¹⁴⁴
- simplified planar models¹⁴⁵
- simplified 3D models¹⁴⁶
- full industrial 3D models¹⁴⁷

Simplified models are usually employed for:

- whole engine dynamics prediction (shaft motions)
- development and validation of new methodologies



► 2D planar model of a fan stage¹⁴⁶

144. S. K. Sinha. en. *International Journal of Non-Linear Mechanics* (2005). doi: [10.1016/j.ijnonlinmec.2004.05.019](https://doi.org/10.1016/j.ijnonlinmec.2004.05.019).

145. M. Legrand et al. en. *Journal of Sound and Vibration* (2009). doi: [10.1016/j.jsv.2008.06.019](https://doi.org/10.1016/j.jsv.2008.06.019).

146. H. Ma et al. en. *Journal of Vibration and Control* (2015). doi: [10.1177/1077546315575835](https://doi.org/10.1177/1077546315575835).

147. N. Guérin et al. en. *Journal of Engineering for Gas Turbines and Power* (2019). doi: [10.1115/1.4040858](https://doi.org/10.1115/1.4040858).

148. A. Batailly et al. en. *Journal of Sound and Vibration* (2015). doi: [10.1016/j.jsv.2015.03.027](https://doi.org/10.1016/j.jsv.2015.03.027).

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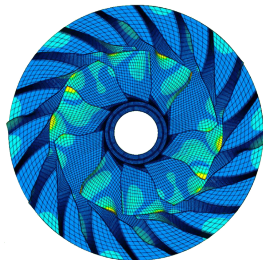
Modelling of the system

Types of models

- analytical models¹⁴⁴
- simplified planar models¹⁴⁵
- simplified 3D models¹⁴⁶
- full industrial 3D models¹⁴⁷

Accurate predictions of the vibration response of bladed disks require full 3D models:

- key for accurate stress levels assessment
- high computational cost ($\sim 10^6$ dof)
- model reduction is required



► 3D model of an impeller¹⁴⁸

144. S. K. Sinha. en. *International Journal of Non-Linear Mechanics* (2005). doi: [10.1016/j.ijnonlinmec.2004.05.019](https://doi.org/10.1016/j.ijnonlinmec.2004.05.019).

145. M. Legrand et al. en. *Journal of Sound and Vibration* (2009). doi: [10.1016/j.jsv.2008.06.019](https://doi.org/10.1016/j.jsv.2008.06.019).

146. H. Ma et al. en. *Journal of Vibration and Control* (2015). doi: [10.1177/1077546315575835](https://doi.org/10.1177/1077546315575835).

147. N. Gu erin et al. en. *Journal of Engineering for Gas Turbines and Power* (2019). doi: [10.1115/1.4040858](https://doi.org/10.1115/1.4040858).

148. A. Batailly et al. en. *Journal of Sound and Vibration* (2015). doi: [10.1016/j.jsv.2015.03.027](https://doi.org/10.1016/j.jsv.2015.03.027).



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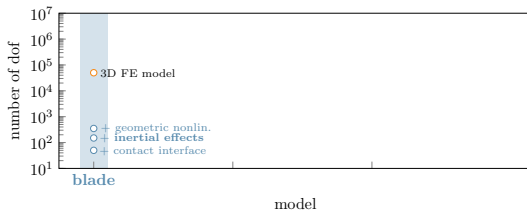
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- industrial 3D FE models (N dof) required for an accurate representation of the contact interface
- numerical efficiency \Rightarrow CMS techniques ($n \ll N$ dof)
- fixed-interface methods are usually preferred for numerical stability¹⁴⁹
- centrifugal stiffening may be accounted for¹⁵⁰ ($n \rightarrow 3n$ dof)
- recent developments (friction modelling and geometric nonlinearities)^{151, 152}

149. R. Bladh et al. *AIAA Journal* (2003). doi: [10.2514/2.2123](https://doi.org/10.2514/2.2123).

150. A. Sternchuss et al. Louvain, 2006, [available online](#).

151. M. Balmaseda et al. en. American Society of Mechanical Engineers Digital Collection, 2019. doi: [10.1115/GT2019-90813](https://doi.org/10.1115/GT2019-90813).

152. E. P. Petrov. en. *Journal of Engineering for Gas Turbines and Power* (2019). doi: [10.1115/1.4045183](https://doi.org/10.1115/1.4045183).



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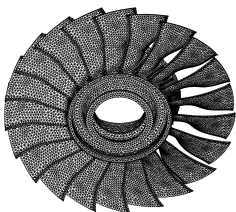
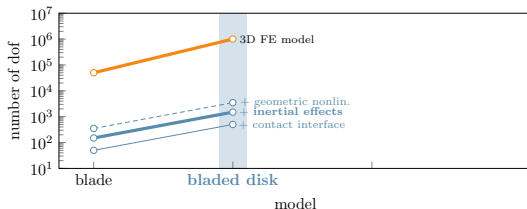
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- property of cyclic symmetry \Rightarrow efficient computation of reduced order models ($10n + \text{dof}$)
- inertial effects may be accounted for¹⁵³ ($30n + \text{dof}$)
- sensitive numerical model due to spurious modes and damping quantification
- recent developments include the combination of mistuning and contact interfaces^{154, 155}
- limited published experimental results involving disk modes have limited the use of such models

153. J. Paltrinieri et al. en. American Society of Mechanical Engineers Digital Collection, 2017. doi: [10.1115/GT2017-63488](https://doi.org/10.1115/GT2017-63488).

154. C. Joannin et al. en. *Journal of Engineering for Gas Turbines and Power* (2016). doi: [10.1115/1.4031886](https://doi.org/10.1115/1.4031886).

155. J. Joachim. fr. PhD thesis. Ecole Polytechnique de Montréal, 2020, OAI: [tel-02888893](https://tel.archives-ouvertes.fr/tel-02888893).



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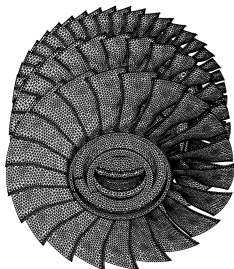
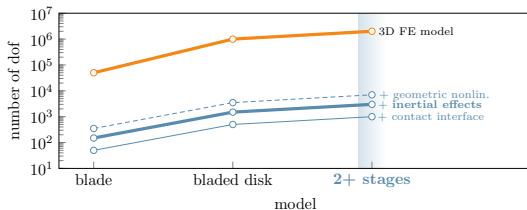
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- multi-stage cyclic symmetry^{156, 157} is the foundation for such numerical models
- inter-stage coupling strategies have also been developed¹⁵⁸
- high numerical cost when combined with time or frequency methods for nonlinear dynamics
- current bottleneck as accurate modelling of the component dynamics is required relevant numerical predictions

156. D. Laxalde et al. en. *Computers & Structures* (2011). doi: [10.1016/j.compstruc.2010.10.020](https://doi.org/10.1016/j.compstruc.2010.10.020).

157. D.-M. Tran. en. *Journal of Sound and Vibration* (2014). doi: [10.1016/j.jsv.2014.06.004](https://doi.org/10.1016/j.jsv.2014.06.004).

158. K. D'Souza et al. *AIAA Journal* (2012). doi: [10.2514/1.J051021](https://doi.org/10.2514/1.J051021).

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Multiphysics simulations

Blade/casing interactions yield intrinsically multiphysics systems

- vibration of the rotor (and the stator)
- wear of the abradable coating ^{159, 160, 161}
- aerodynamic loading in engine conditions
 - ▶ interactions experimentally observed under vacuum ¹⁶²
 - ▶ when accounted for, simplified loadings ¹⁶³
- thermomechanics ^{164, 165} (extreme temperature in turbine stages)

160. M. Legrand et al. en. *Journal of Computational and Nonlinear Dynamics* (2012). doi: [10.1115/1.4004951](https://doi.org/10.1115/1.4004951).

161. R. J. Williams. en. American Society of Mechanical Engineers Digital Collection, 2012. doi: [10.1115/GT2011-45495](https://doi.org/10.1115/GT2011-45495).

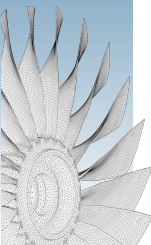
162. P. Almeida et al. en. *Journal of Engineering for Gas Turbines and Power* (2016). doi: [10.1115/1.4033065](https://doi.org/10.1115/1.4033065).

163. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2010. doi: [10.1115/DETC2009-86842](https://doi.org/10.1115/DETC2009-86842).

164. A. Batailly et al. en. American Society of Mechanical Engineers Digital Collection, 2014. doi: [10.1115/GT2014-25675](https://doi.org/10.1115/GT2014-25675).

165. Q. Agrapart et al. en. *Journal of Sound and Vibration* (2019). doi: [10.1016/j.jsv.2019.114869](https://doi.org/10.1016/j.jsv.2019.114869).

166. F. Nyssen et al. en. *Journal of Engineering for Gas Turbines and Power* (2019). doi: [10.1115/1.4041647](https://doi.org/10.1115/1.4041647).



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⇒ mostly a computational challenge

160. M. Legrand et al. en. *Journal of Computational and Nonlinear Dynamics* (2012). doi: [10.1115/1.4004951](https://doi.org/10.1115/1.4004951).

161. R. J. Williams. en. American Society of Mechanical Engineers Digital Collection, 2012. doi: [10.1115/GT2011-45495](https://doi.org/10.1115/GT2011-45495).

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163. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2010. doi: [10.1115/DETC2009-86842](https://doi.org/10.1115/DETC2009-86842).

164. A. Batailly et al. en. American Society of Mechanical Engineers Digital Collection, 2014. doi: [10.1115/GT2014-25675](https://doi.org/10.1115/GT2014-25675).

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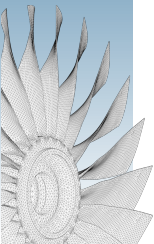
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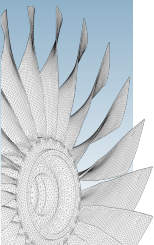
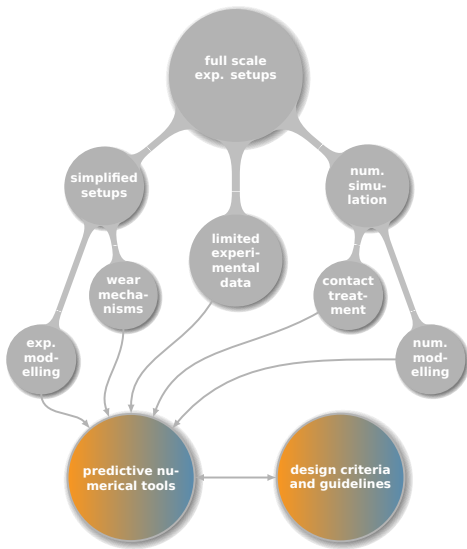
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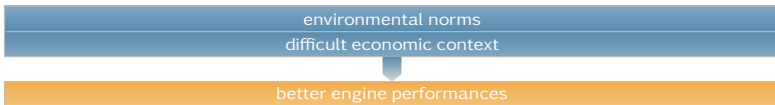
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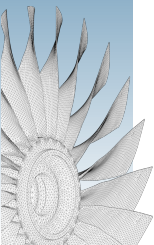
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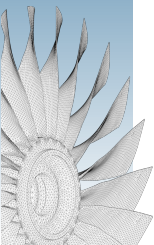
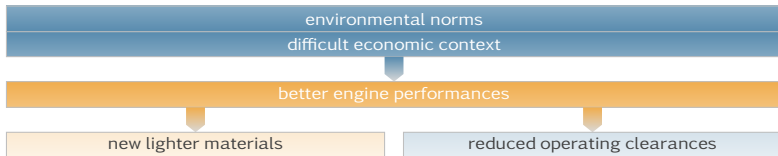
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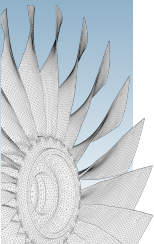
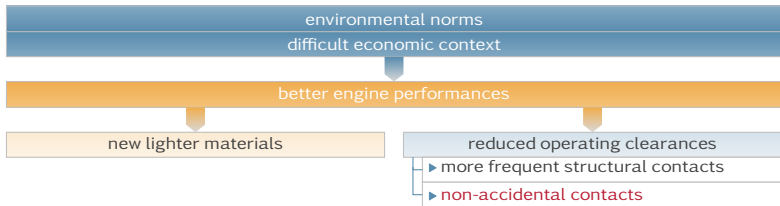
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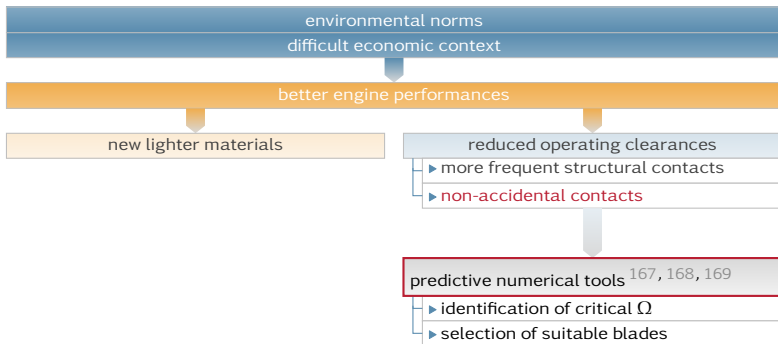
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167. E. P. Petrov et al. en. *Journal of Turbomachinery* (2004). doi: [10.1115/1.1644557](https://doi.org/10.1115/1.1644557).

168. F. El Haddad et al. Glasgow, Scotland, 2018, [online reference](#).

169. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2015. doi: [10.1115/GT2015-42682](https://doi.org/10.1115/GT2015-42682).



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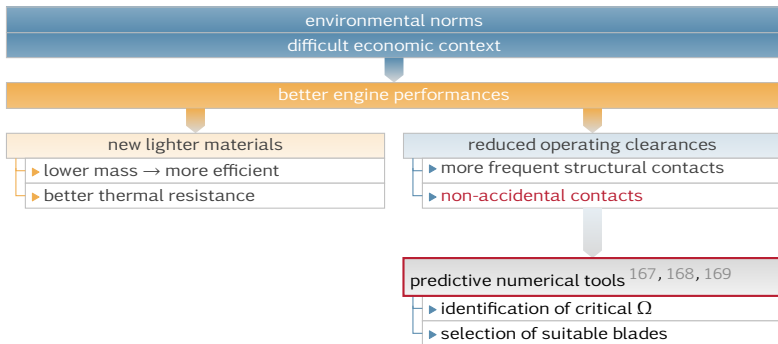
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Industrial context: today



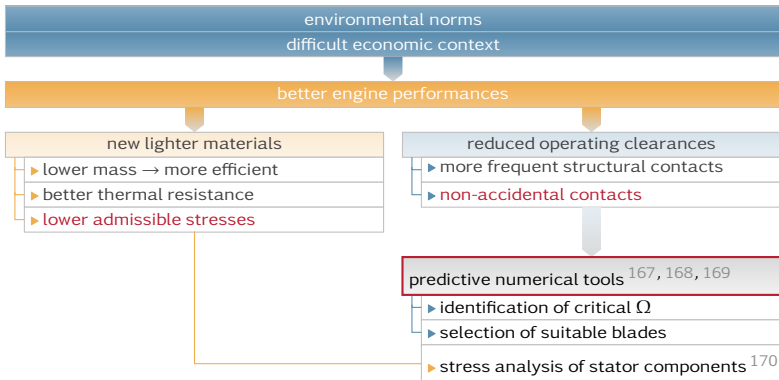
167. E. P. Petrov et al. en. *Journal of Turbomachinery* (2004). doi: [10.1115/1.1644557](https://doi.org/10.1115/1.1644557).

168. F. El Haddad et al. Glasgow, Scotland, 2018, [online reference](#).

169. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2015. doi: [10.1115/GT2015-42682](https://doi.org/10.1115/GT2015-42682).



Industrial context: today



167. E. P. Petrov et al. en. *Journal of Turbomachinery* (2004). doi: [10.1115/1.1644557](https://doi.org/10.1115/1.1644557).

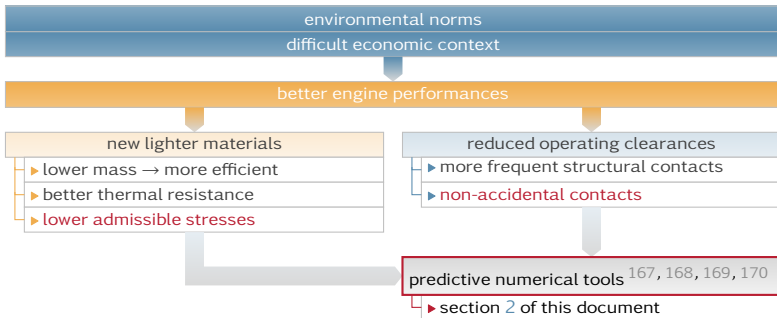
168. F. El Haddad et al. Glasgow, Scotland, 2018, [online reference](#).

169. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2015. doi: [10.1115/GT2015-42682](https://doi.org/10.1115/GT2015-42682).

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Industrial context: today



167. E. P. Petrov et al. en. *Journal of Turbomachinery* (2004). doi: [10.1115/1.1644557](https://doi.org/10.1115/1.1644557).

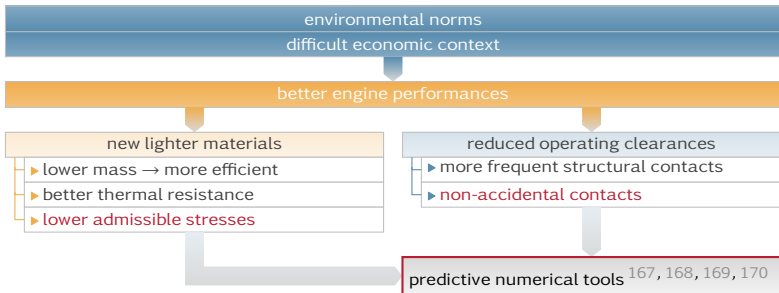
168. F. El Haddad et al. Glasgow, Scotland, 2018, [online reference](#).

169. A. Millecamps et al. en. American Society of Mechanical Engineers Digital Collection, 2015. doi: [10.1115/GT2015-42682](https://doi.org/10.1115/GT2015-42682).

170. F. Nyssen et al. en. *Journal of Sound and Vibration* (2020). doi: [10.1016/j.jsv.2019.115040](https://doi.org/10.1016/j.jsv.2019.115040).



Industrial context: today



1

2

3

167. E. P. Petrov et al. en. *Journal of Turbomachinery* (2004). doi: [10.1115/1.1644557](https://doi.org/10.1115/1.1644557).

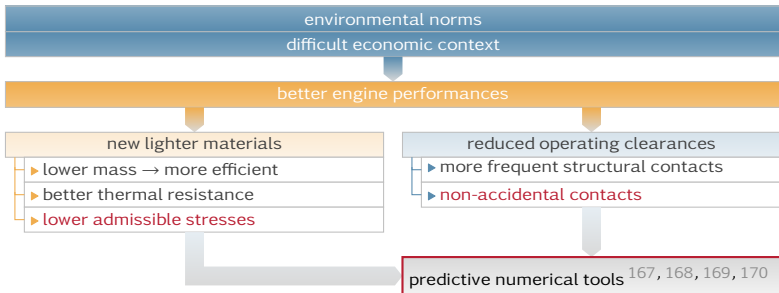
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Industrial context: today



① today: a *a posteriori* discrimination of blade profiles (response to contact)

②

③

167. E. P. Petrov et al. en. *Journal of Turbomachinery* (2004). doi: [10.1115/1.1644557](https://doi.org/10.1115/1.1644557).

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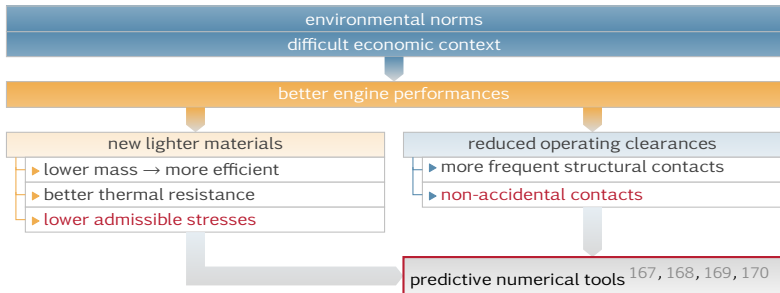
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- 1 today: a *a posteriori* discrimination of blade profiles (response to contact)
- 2 in progress: account for contact during blades design stage (constraint)¹⁷¹
- 3

167. E. P. Petrov et al. en. *Journal of Turbomachinery* (2004). doi: [10.1115/1.1644557](https://doi.org/10.1115/1.1644557).

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171. A. Batailly et al. en. *Journal of Engineering for Gas Turbines and Power* (2015). doi: [10.1115/1.4028263](https://doi.org/10.1115/1.4028263).



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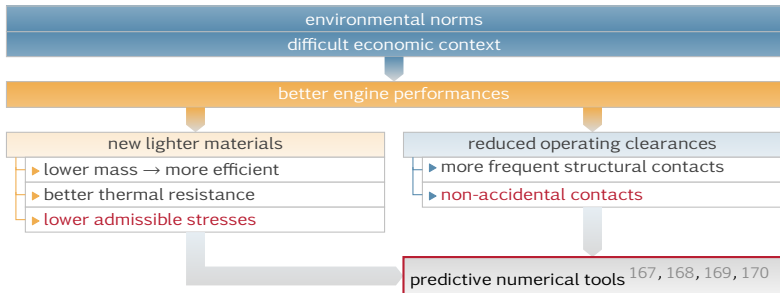
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Industrial context: today



- 1 today: a *a posteriori* discrimination of blade profiles (response to contact)
- 2 in progress: account for contact during blades design stage (constraint)¹⁷¹
- 3 future: define new design criteria and guidelines for robust blades with respect to contact interactions

167. E. P. Petrov et al. en. *Journal of Turbomachinery* (2004). doi: [10.1115/1.1644557](https://doi.org/10.1115/1.1644557).

168. F. El Haddad et al. Glasgow, Scotland, 2018, [online reference](#).

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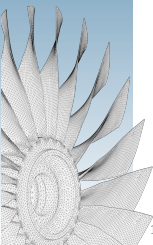
References

Accounting for contact in blade design

Current design strategies

- emphasis on aerodynamic performances
- need for minimal operating clearances
- recent design recommendations promote blade profiles that reduce operating clearances as they vibrate¹⁷²
- nonlinear dynamics considerations may only be accounted for *a posteriori*

⇒ significant cost as existing predictive tools can only be used to discriminate existing blade profiles based on their response to contact





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Accounting for contact in blade design

Current design strategies

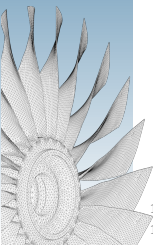
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⇒ opposition between aerodynamics and nonlinear dynamics considerations^{172, 173}

172. E. Erler et al. en. *Journal of Turbomachinery* (2016). doi: [10.1115/1.4031865](https://doi.org/10.1115/1.4031865).

173. A. Batailly et al. en. *Journal of Engineering for Gas Turbines and Power* (2015). doi: [10.1115/1.4028263](https://doi.org/10.1115/1.4028263).





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⇒ significant cost as existing predictive tools can only be used to discriminate existing blade profiles based on their response to contact

⇒ opposition between aerodynamics and nonlinear dynamics considerations^{172, 173}

⇒ contact must be accounted for early in the blade design stage

172. E. Erler et al. en. *Journal of Turbomachinery* (2016). doi: [10.1115/1.4031865](https://doi.org/10.1115/1.4031865).

173. A. Batailly et al. en. *Journal of Engineering for Gas Turbines and Power* (2015). doi: [10.1115/1.4028263](https://doi.org/10.1115/1.4028263).



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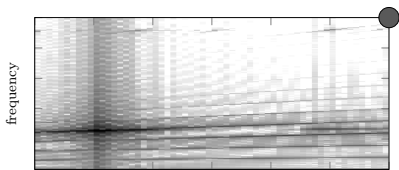
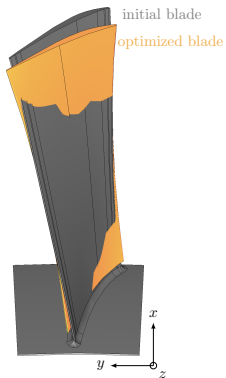
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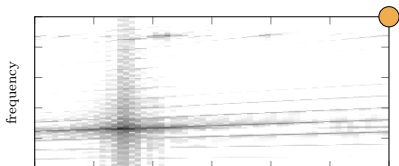
References

Development of automated optimization procedures

- based on existing design criteria¹⁷⁴
- reverse engineering of existing blade profiles and optimization



angular speed



angular speed



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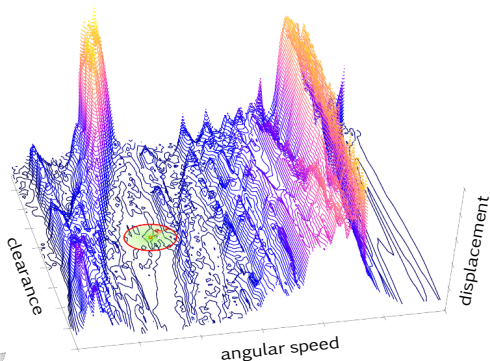
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Accounting for contact in blade design

Development of new optimization algorithms

- new optimization techniques are required for nonsmooth objective functions¹⁷⁵
- optimal design points must be found *far enough* from potential bifurcations in the space of variables
- blackbox optimization framework well-suited for costly industrial procedures





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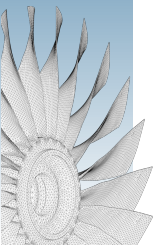
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III - Industrial
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**IV - Going
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④ Going forward...





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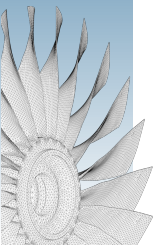
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On-going research and future directions

Several open questions

- understanding of complex wear mechanisms
- better understand the physics of the phenomena (thermomechanics)
- development of more efficient numerical solution strategies
- use of high fidelity industrial multi-stage models
- assess the robustness of numerical predictions to uncertainties





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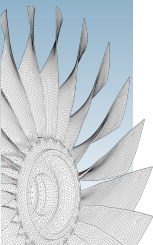
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One major road block

- accurate numerical predictions require test data ⇒ **very few available**
- selection of a suitable wear law requires test data ⇒ **mostly confidential**
- characterization of new lighter materials is limited due to **confidentiality**
- components design itself is often **confidential**





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On-going research and future directions

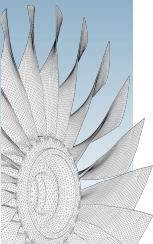
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- components design itself is often **confidential**

⇒ it is, most of the time, **impossible to reproduce published results**





On-going research and future directions

Several open questions

- understanding of complex wear mechanisms
- better understand the physics of the phenomena (thermomechanics)
- development of more efficient numerical solution strategies
- use of high fidelity industrial multi-stage models
- assess the robustness of numerical predictions to uncertainties

Promoting data exchange and numerical comparisons

- publications as open archives (or in open access journals) are not the only solution



- promote the dissemination of numerical tools^{176, 177} ⇒ open source



Software Heritage platform

- use of standardized test cases¹⁷⁸ (see CFD code validations in the 1990s) ⇒ open blade models

178. E. Piollet et al. en. *Journal of Sound and Vibration* (2019). doi: 10.1016/j.jsv.2019.114878.

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Thank you for your attention!

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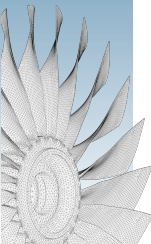
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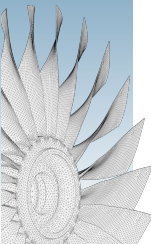
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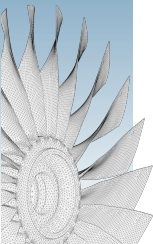
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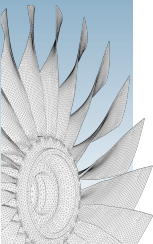


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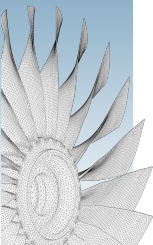


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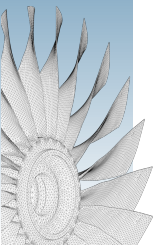
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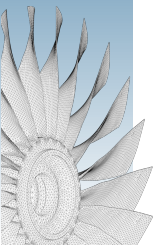
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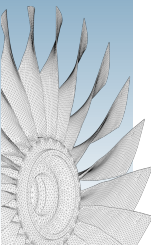
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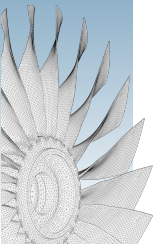


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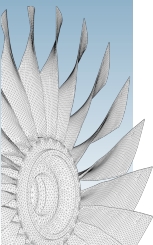
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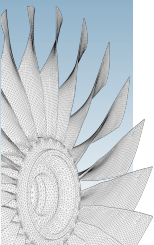
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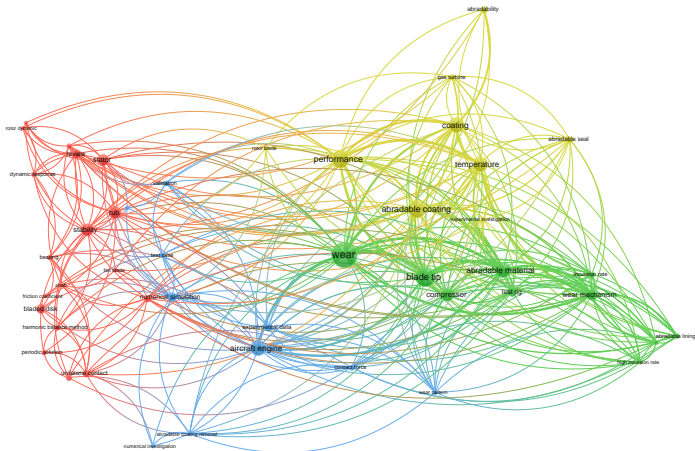
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