

Rotor 51A

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About

This report presents the experimental performance for a fan in the series, designated fan stage 51A. The 12-bladed, 50.8-centimeter-diameter fan was designed for a tip-speed of 243.8 meters per second. The design stage pressure ratio was 1.15 at a weight flow of 29.9 kilograms per second. The fan blade angles can be manually reset. Overall performance for both the rotor and the stage along with the blade-element performance of both rotor and stator are presented for the design rotor blade setting angle.

- Original NASA technical report ^[1]:

```
@TechReport{osborn1974performance,
  author      = {Osborn, Walter Martin and Steinke, Ronald J},
  date       = {1974},
  institution = {NASA Lewis Research Center Cleveland, OH, United
States},
  title      = {Performance of a 1.15-pressure-ratio Axial-flow Fan
Stage with a Blade Tip Solidity of 0.5},
  number     = {NASA-TM X-3052},
  url       = {https://ntrs.nasa.gov/citations/19740021256},
}
```

- Pictures :



Fig1. <https://ntrs.nasa.gov/citations/19740021256> p.67



Fig2. <https://ntrs.nasa.gov/citations/19740021256> p.67

Useful documents

- [downloadable models](#) (Git project)
 - NASA technical report (.pdf)
 - rotor51a_original.csv (.csv), usable as input of OpenMCAD^[2] to generate reference blade models.

Reference blade

The **reference blade** is defined with multiple-circular arc profiles^[3] given in the original NASA report^[1]. Corresponding models are computed with the open-source code OpenMCAD^[2].

Geometry

The geometry of rotor 51A is described in the [original NASA report](#) by the following table. The lengths are in inches and the angles in degrees.

TABLE IV. - BLADE GEOMETRY FOR ROTOR 51A

| SPAN | RADII | | BLADE ANGLES | | | DELTA INC | CONE ANGLE |
|------|--------|--------|--------------|-------|-------|-----------|------------|
| | R1 | R2 | KTC | KTT | KCC | | |
| 0.00 | 25.411 | 25.411 | 52.15 | 47.66 | 45.1 | 4.59 | 0.057 |
| 0.05 | 24.628 | 24.628 | 51.73 | 46.66 | 43.19 | 4.63 | -0.130 |
| 0.10 | 23.845 | 23.845 | 51.30 | 45.66 | 41.52 | 4.66 | 0.057 |
| 0.15 | 23.062 | 23.062 | 49.86 | 44.16 | 39.66 | 5.43 | 0.268 |
| 0.20 | 22.279 | 22.279 | 46.26 | 40.16 | 35.43 | 7.12 | 0.997 |
| 0.25 | 21.496 | 21.496 | 41.54 | 35.16 | 24.67 | 11.69 | 1.605 |
| 0.30 | 20.713 | 20.713 | 35.62 | 29.16 | 14.63 | 15.64 | 2.092 |
| 0.35 | 19.930 | 19.930 | 28.21 | 23.16 | 7.15 | 17.75 | 1.619 |
| 0.40 | 19.147 | 19.147 | 20.46 | 17.16 | 4.03 | 18.29 | 1.274 |
| 0.45 | 18.364 | 18.364 | 12.65 | 11.16 | 2.57 | 18.29 | 0.654 |
| 0.50 | 17.581 | 17.581 | 5.91 | 5.12 | 1.01 | 16.46 | 0.057 |

| SPAN | BLADE THICKNESSES | | AXIAL DIMENSIONS | | |
|------|-------------------|------|------------------|------|------|
| | T1 | T2 | Z1 | Z2 | Z3 |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.35 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.40 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.45 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

Aerodynamic design

| | unit | value |
|----------------|--------|-----------------------------|
| pressure ratio | [-] | 1.111 |
| mass flow | [kg/s] | 30.27 |
| tip speed | [m/s] | 213,3 |
| tip solidity | [-] | 0.5 |
| aspect ratio | [-] | 3.08 |
| rotative speed | [%] | 90 to 120 % of design speed |

Material properties

The material of rotor 51A is not defined in the original NASA report. A 200-grade maraging steel is considered:

| | unit | value |
|-----------------|---------|--------------------|
| alloy | [-] | 18-Ni-200-maraging |
| Young's modulus | [GPa] | 180 |
| density | [kg/m3] | 8000 |

| | unit | value |
|------------------------|-------------|--------------|
| Poisson's ratio | [-] | 0.3 |
| yield stress | [GPa] | 1.38 |

CAD model

The CAD model is computed with the open source code OpenMCAD^[2].



pressure side



suction side

Natural frequencies

First three natural frequencies (with clamped root) for the mesh computed with OpenMCAD^[2]:

| Mode | Type | Natural angular frequency (rad/sec) | Natural frequency (Hz) |
|-------------|-------------|--|-------------------------------|
| 1 | | 2578.588 | 410.395 |
| 2 | | 8044.80 | 1280.37 |
| 3 | | 10763.98 | 1713.14 |

Initial blade

The **initial blade** is defined with in-house LAVA parameters^[4] computed from the reference blade CAD model. The initial blade is usually used as starting point for an optimization process. Its geometry is similar to the one of the reference blade.

Natural frequencies

First three natural frequencies (with clamped root)

- from the whole mesh:

| Mode | Type | Natural angular frequency (rad/sec) | Natural frequency (Hz) |
|------|------|-------------------------------------|------------------------|
| 1 | | 2560.66 | 407.541 |
| 2 | | 8009.99 | 1 274.83 |
| 3 | | 10726.52 | 1 707.18 |

- from the reduced order model:

| Mode | Type | Natural angular frequency (rad/sec) | Natural frequency (Hz) |
|------|------|-------------------------------------|------------------------|
| 1 | | 2560.75 | 407.556 |
| 2 | | 8013.95 | 1275.46 |
| 3 | | 10729.8 | 1707.7 |

Modèles téléchargeables

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Libre accès

[lien vers le projet Git](#)

À propos

Ce rapport présente les performances expérimentales d'un ventilateur de la série, désigné étage de ventilateur 51A. Le ventilateur à 12 pales de 50,8 centimètres de diamètre a été conçu pour une vitesse de pointe de 243,8 mètres par seconde. La pression d'étage de conception était de 1,15 à un débit pondéral de 29,9 kilogrammes par seconde. Les angles des pales du ventilateur peuvent être réinitialisés manuellement. Performances globales pour le rotor. Les performances du rotor et du stator sont présentées pour l'angle de réglage des pales du rotor de conception.

- Rapport technique original ^[1]:

```
@TechReport{osborn1974performance,
  author      = {Osborn, Walter Martin and Steinke, Ronald J},
  date       = {1974},
  institution = {NASA Lewis Research Center Cleveland, OH, United States},
```

```
title = {Performance of a 1.15-pressure-ratio Axial-flow Fan  
Stage with a Blade Tip Solidity of 0.5},  
number = {NASA-TM X-3052},  
url = {https://ntrs.nasa.gov/citations/19740021256},  
}
```

- Photographies :

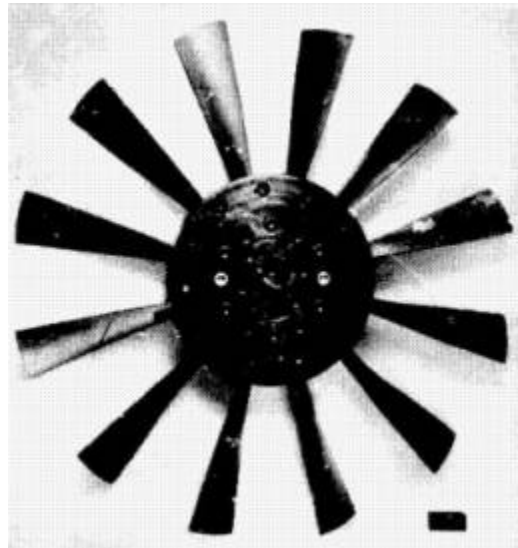


Fig1. <https://ntrs.nasa.gov/citations/19740021256> p.67

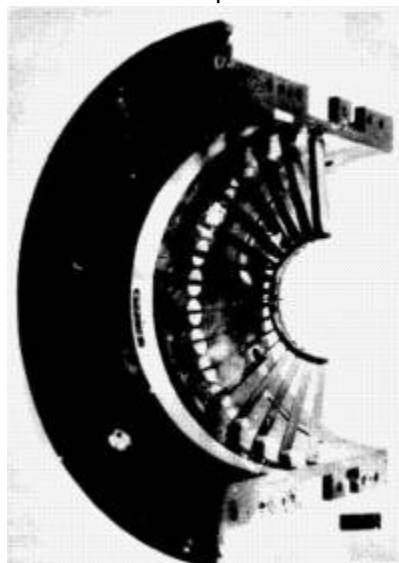


Fig2. <https://ntrs.nasa.gov/citations/19740021256> p.67

Documents utiles

- [modèles téléchargeables](#) (lien vers projet Git)
 - rapport technique original de la NASA (.pdf)
 - rotor51a_original.csv (.csv), utilisable en entrée de OpenMCAD^[2] pour générer l'aube de référence

Aube de référence

L'**aube de référence** est définie par des profils de type arcs circulaires multiples^[3], donnés dans le rapport technique original de la NASA^[1]. Les modèles associés sont obtenus avec le code en libre accès OpenMCAD^[2].

Géométrie

La géométrie du rotor 51A est décrite dans le rapport d'origine de la NASA par les tableaux suivants. Les grandeurs sont en pouces et en degrés.

TABLE IV. - BLADE GEOMETRY FOR ROTOR 51A

| RD | PERCENT SPAN | | RADIUS | | BLADE ANGLES | | | DELTA INC | CONE ANGLE |
|----|--------------|---------|---------|-------|--------------|-------|-------|-----------|------------|
| | SPAN | R1 | R2 | KTC | K7 | KCC | | | |
| 10 | 100 | 100 | 100 | 100 | 52.15 | 47.60 | 43.10 | 4.50 | 0.057 |
| 90 | 95 | 92.6470 | 92.6356 | 91.23 | 46.60 | 43.10 | 4.60 | -0.130 | |
| 80 | 90 | 85.6730 | 85.6700 | 80.20 | 45.00 | 41.50 | 4.60 | 0.057 | |
| 70 | 85 | 75.9500 | 75.9440 | 70.10 | 42.00 | 38.00 | 5.45 | 0.258 | |
| 60 | 80 | 67.4240 | 67.4200 | 60.00 | 40.00 | 35.00 | 7.70 | 0.997 | |
| 50 | 75 | 59.8950 | 59.8900 | 50.00 | 38.00 | 34.00 | 11.00 | 1.805 | |
| 40 | 70 | 52.3650 | 52.3600 | 40.00 | 35.00 | 32.00 | 15.00 | 2.000 | |
| 30 | 65 | 44.8350 | 44.8300 | 30.00 | 32.00 | 30.00 | 17.75 | 1.610 | |
| 20 | 60 | 37.3050 | 37.3000 | 20.00 | 28.00 | 28.00 | 16.10 | 1.274 | |
| 10 | 55 | 29.7750 | 29.7700 | 10.00 | 24.00 | 26.00 | 16.20 | 0.634 | |
| 0 | 50 | 22.2450 | 22.2400 | 0.00 | 20.00 | 24.00 | 16.40 | 0.057 | |

| RD | BLADE THICKNESSES | | | AXIAL DIMENSIONS | | |
|----|-------------------|-------|-------|------------------|-------|-------|
| | Z1 | Z2 | Z3 | Z1 | Z2 | Z3 |
| 10 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 90 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 80 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 20 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 10 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

Caractéristiques aérodynamiques

| | unité | valeurs |
|----------------------------|--------|--|
| taux de compression | [-] | 1.111 |
| débit massique | [kg/s] | 30.27 |
| vitesse en tête | [m/s] | 213,3 |
| solidité en tête | [-] | 0.5 |
| allongement | [-] | 3.08 |
| vitesse de rotation | [%] | 90 à 120 % de la vitesse de conception |

Propriétés matériau

Le matériau original du rotor 51A n'est pas défini dans le rapport de la NASA. Un alliage de titane Ti-6Al-4v est considéré :

| | unités | valeurs |
|-------------------------------|----------------------|-----------|
| alliage | [-] | Ti-6Al-4V |
| module d'Young | [GPa] | 108 |
| masse volumique | [kg/m ³] | 4400 |
| coefficient de Poisson | [-] | 0,34 |
| limite élastique | [GPa] | 0,824 |

Modèle CAO

Le modèle CAO est obtenu avec OpenMCAD^[2].

intrados



extrados



Fréquences propres

Fréquences des trois premiers modes (noeuds du pied d'aube encastres) pour le maillage obtenu avec OpenMCAD^[2] :

| Mode | Type | Pulsation propre (rad/sec) | Fréquence propre (Hz) |
|------|------|----------------------------|-----------------------|
| 1 | | 2578,588 | 410,395 |
| 2 | | 8044,80 | 1280,37 |
| 3 | | 10763,98 | 1713,14 |

Aube initiale

L'**aube initiale** est définie par des paramètres spécifiques au LAVA^[4] obtenus à partir du modèle CAO de l'aube de référence. L'aube initiale est classiquement utilisée comme point de départ dans le cadre de procédures d'optimisation; sa géométrie est similaire à celle de l'aube de référence.

Fréquences propres

Fréquences des trois premiers modes (noeuds du pied d'aube encastres),

- pour le maillage complet :

| Mode | Type | Pulsation propre (rad/sec) | Fréquence propre (Hz) |
|------|------|----------------------------|-----------------------|
| 1 | | 2560,66 | 407,541 |
| 2 | | 8009,99 | 1 274,83 |
| 3 | | 10726,52 | 1 707,18 |

- pour le modèle réduit :

| Mode | Type | Pulsation propre (rad/sec) | Fréquence propre (Hz) |
|------|------|----------------------------|-----------------------|
| 1 | | 2560,75 | 407,556 |
| 2 | | 8013,95 | 1275,46 |
| 3 | | 10729,8 | 1707,7 |

1. ^{a, b, c, d} «Performance of a 1.15-pressure-ratio Axial-flow Fan Stage with a Blade Tip Solidity of 0.5» 1974. [pdf](#)
2. ^{a, b, c, d, e, f, g, h} Kojtych S., Batailly A. «OpenMCAD, an open blade generator: from Multiple-Circular-Arc profiles to Computer-Aided Design model» 2022. [code en libre accès](#)
3. ^{a, b} Crouse *et al.* «A computer program for composing compressor blading from simulated circular-arc elements on conical surfaces » 1969. NASA-TN-D-5437. [pdf](#)
4. ^{a, b} Kojtych S. *et al.* «Methodology for the Redesign of Compressor Blades Undergoing Nonlinear Structural Interactions: Application to Blade-Tip/Casing Contacts » 2022. Journal of Engineering for Gas Turbines and Power, Vol. 145, No. 5. [pdf](#)

Document issu de la page wiki:

https://lava-wiki.meca.polymtl.ca/public/modeles/rotor_51a/accueil?rev=1681493358

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